

FIELD BOOK

364

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

PLEASE RETURN TO
GEOGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
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32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Jullon A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

Book 45

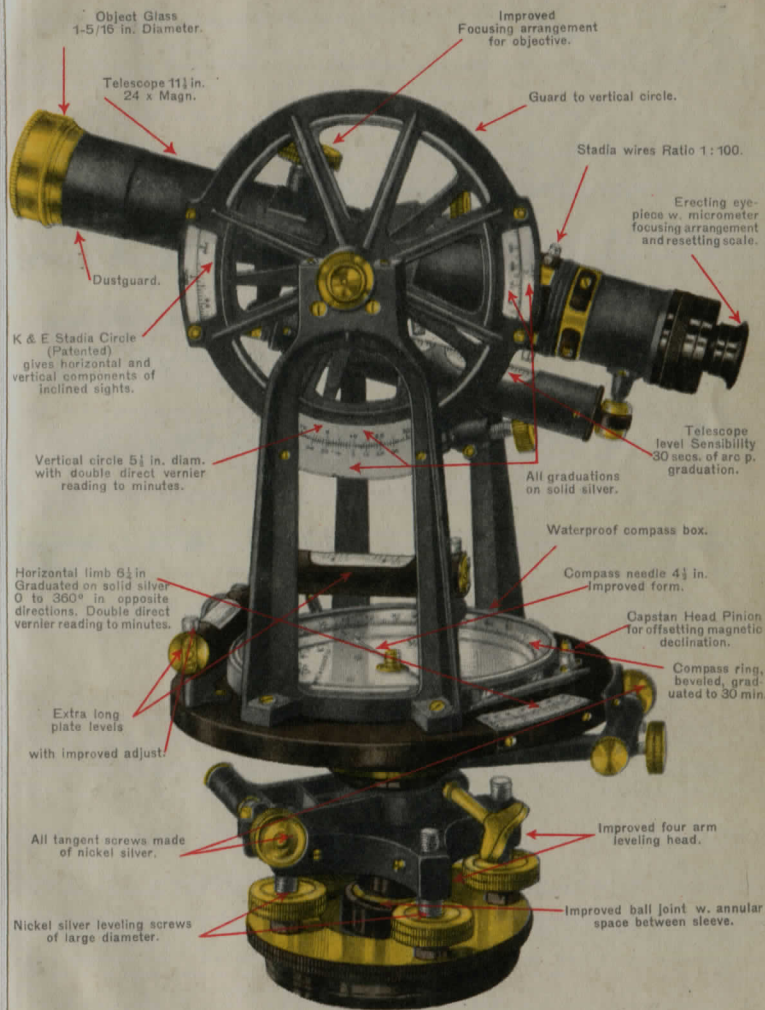
4519

Section A.
Cuyahoga - Geauga
County Line Road from
Mulberry Corners Road N to
Lake Co. Line - Page 1
Piety
Data on Puckerbrush
T.H. 9594
Road, Chester Twp. Page 15
Location and Levels on County
Highway No 4 North of Center Chardon
(Stafford Hill) Page 11
"Chester Excav." " 18
Cuyahoga - Geauga County Line Road
Section B. from Wilson Mills Rd North
Page 26
Piety Rd. & Location Page 37
#4 SEC'S O.P.R. Pg 36 Twp SEC'S

AUBURN RD. #4 STU 1951

Pgs 37-

EXTRA FINE ENGINEERS' TRANSIT
No. 5060 S
KEUFFEL & ESSER CO., N.Y.



ALSO MADE WITH

INTERNAL FOCUSING TELESCOPE
PRACTICALLY DUST AND MOISTURE PROOF. -

COUNTY LINE
ROAD FROM MULBERRY
COR. ROAD NORTH

T.H. 93

→ = pg 1 to 10

Chardon-Auburn Rd (Chardon Center
North to Co. Line ✓ pg 11 to 14
" 37 " 39

Brook Lane
Ferry Rd (N.W. Chester ✓ pg 15

County Line Rd (Wilson Mills to Mulberry Rd ✓ pg 26

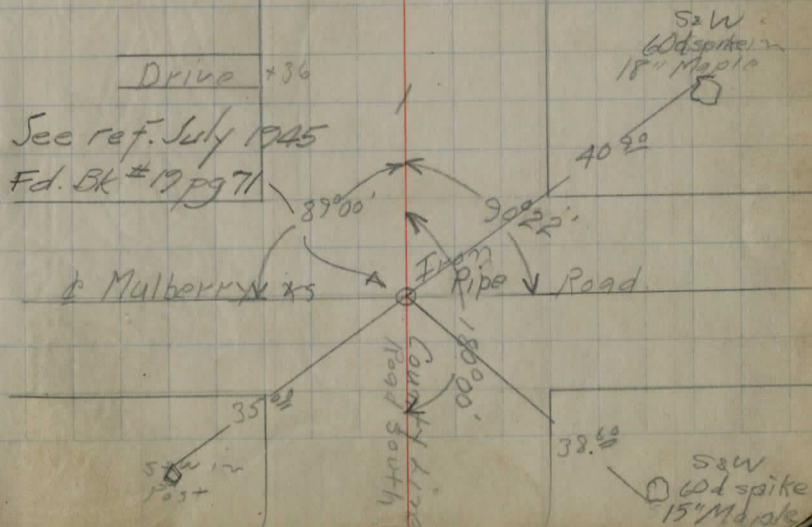
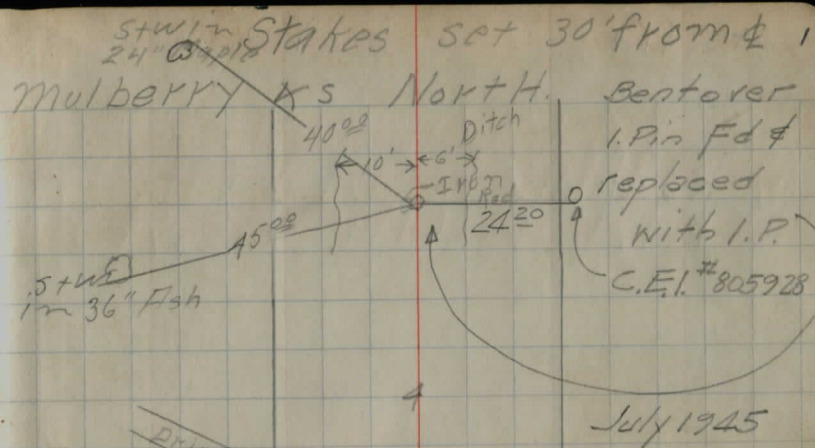
Ferry
Pietz Rd pg 32

Drainage LEVELS N. END CH. 4 19

LEVELS CH. 4 20-25

Section A
County Line Rd from

Sta 5+00 POT Def 0°00' Iron Rod



Sta 0+00

Iron pipe

x x x x x $\frac{53}{30}$

11

Ditch
 14' 10' 4'

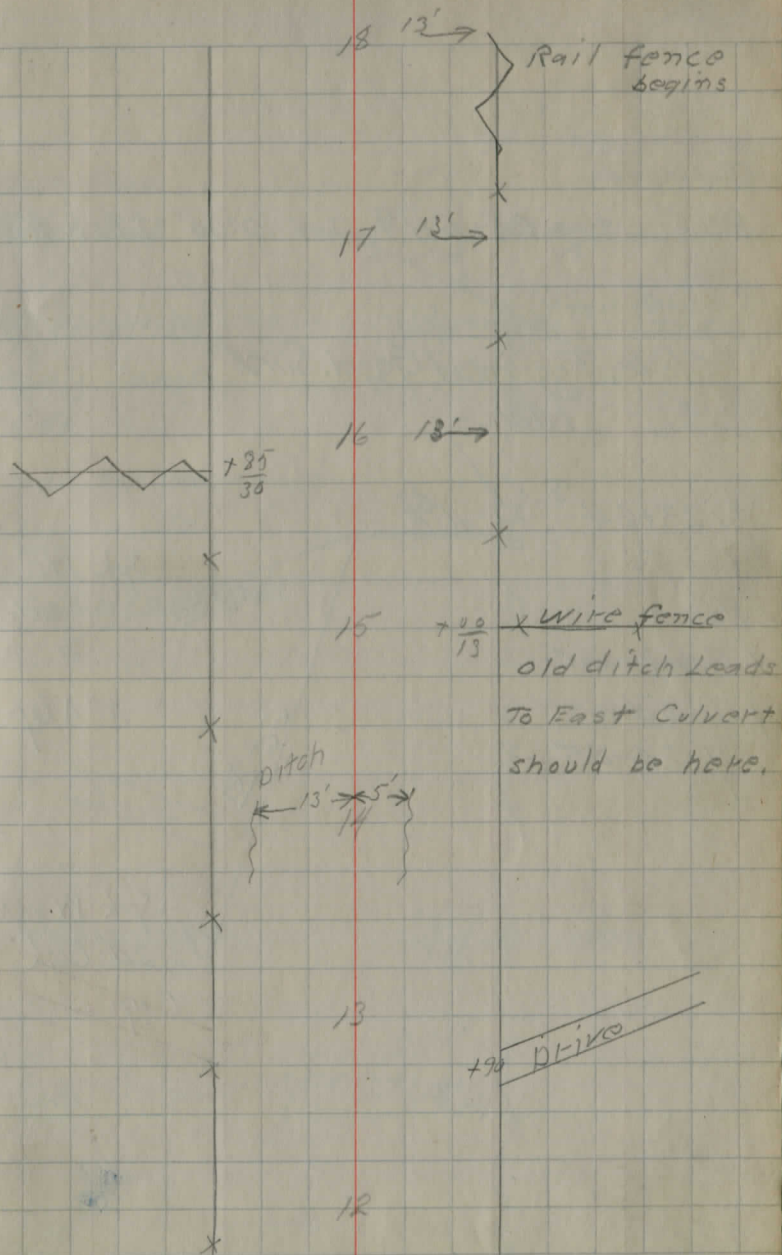
9

~~15~~
12

8

7

6



POT Sta 23+64¹⁰ Def 0°00' From Rod

Cleve. Regional Geod. Surv.

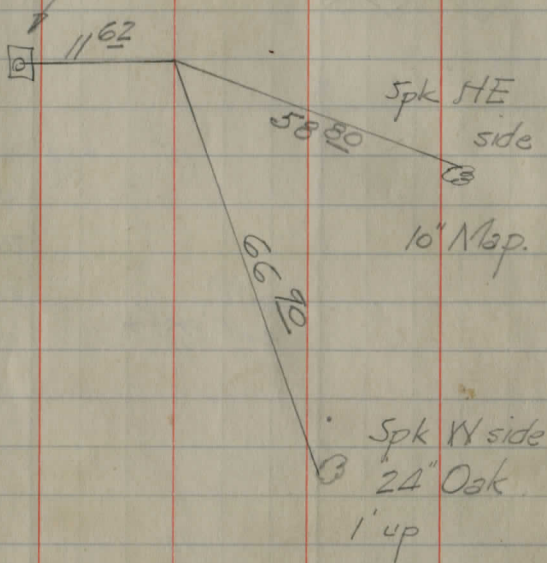
Mon.

Sta 23+64¹⁰

1. Pin fd
1' down

1. P set over
pin 3" down

7-24-45



side Road
culvert 2'x2'
stone Box 171
fair Condition
overall Length
30.5 ft
Box 11' from E
of Co. Line Rd.

DRIVE +80

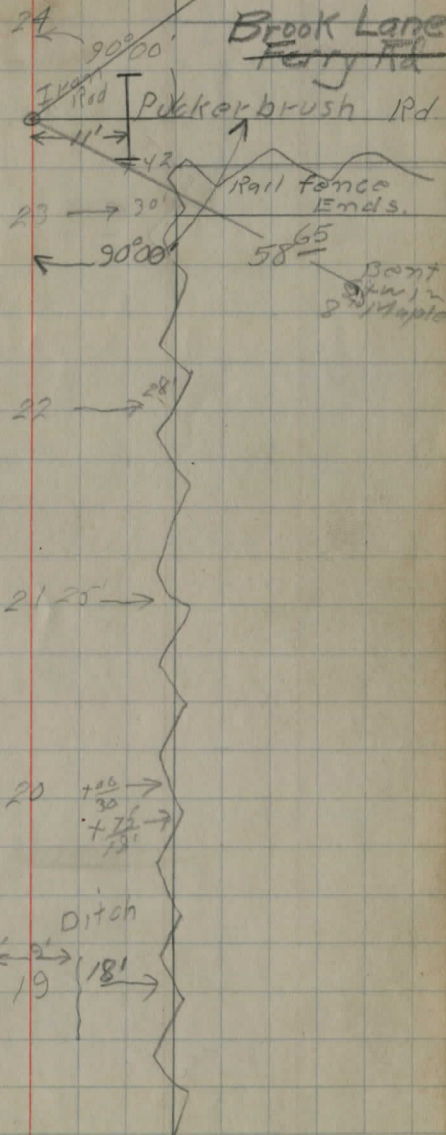
DRIVE +45

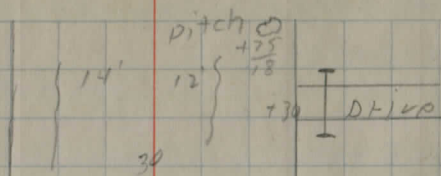
Ditch
18' →
19' →

5' x 1/2" x cherry

46.75

Brook Lane
Ferry Rd





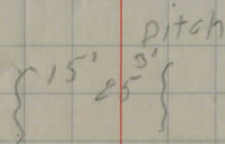
15" I.P. Drive
way 15.5' Long
12' From $\frac{1}{2}$.

29

28

27

26



37

Sta 37+00

Stake set 35'

36

Sta 36+00 Stake

set 35' from $\frac{1}{2}$

35

Sta 35+00 Stake

set 35' from $\frac{1}{2}$

+77

Drive

34

 $\frac{+66}{25}$

33

 $\frac{+25}{25}$ $\frac{+14}{25}$

32

 $\frac{+25}{25}$ $\frac{+66}{25}$ $\frac{+18}{18}$

31

 $\frac{+25}{18}$

49

48

47

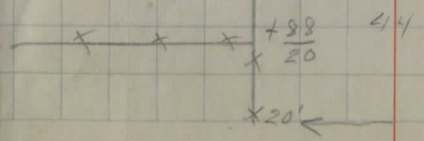
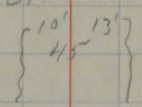
46

+55
20

+45
20

+35
20

Ditch



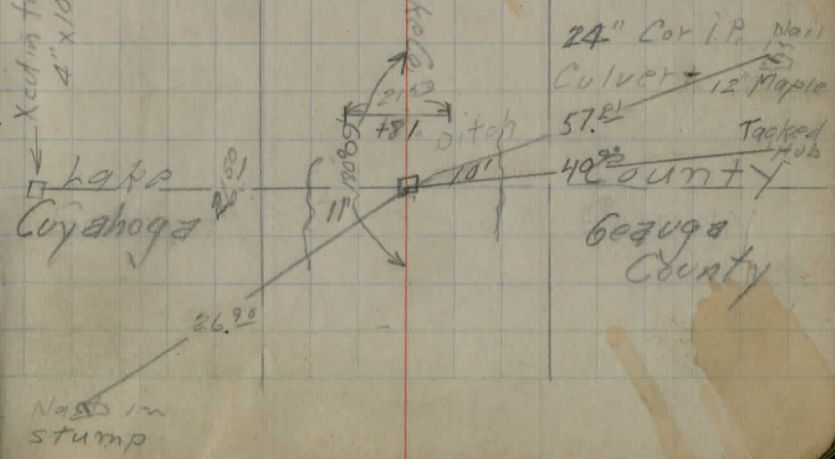
End of project stg 49 + 75⁴⁵ Found
Iron Red in top of wood Hub

94 mi

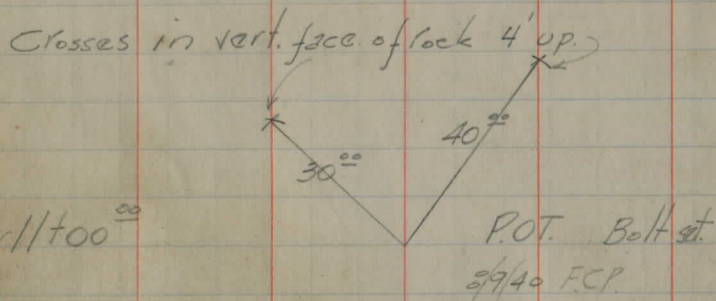
X cut in top of cut stone
4" x 10"

Lake
Cuyahoga

County Line Rd N to Lakota



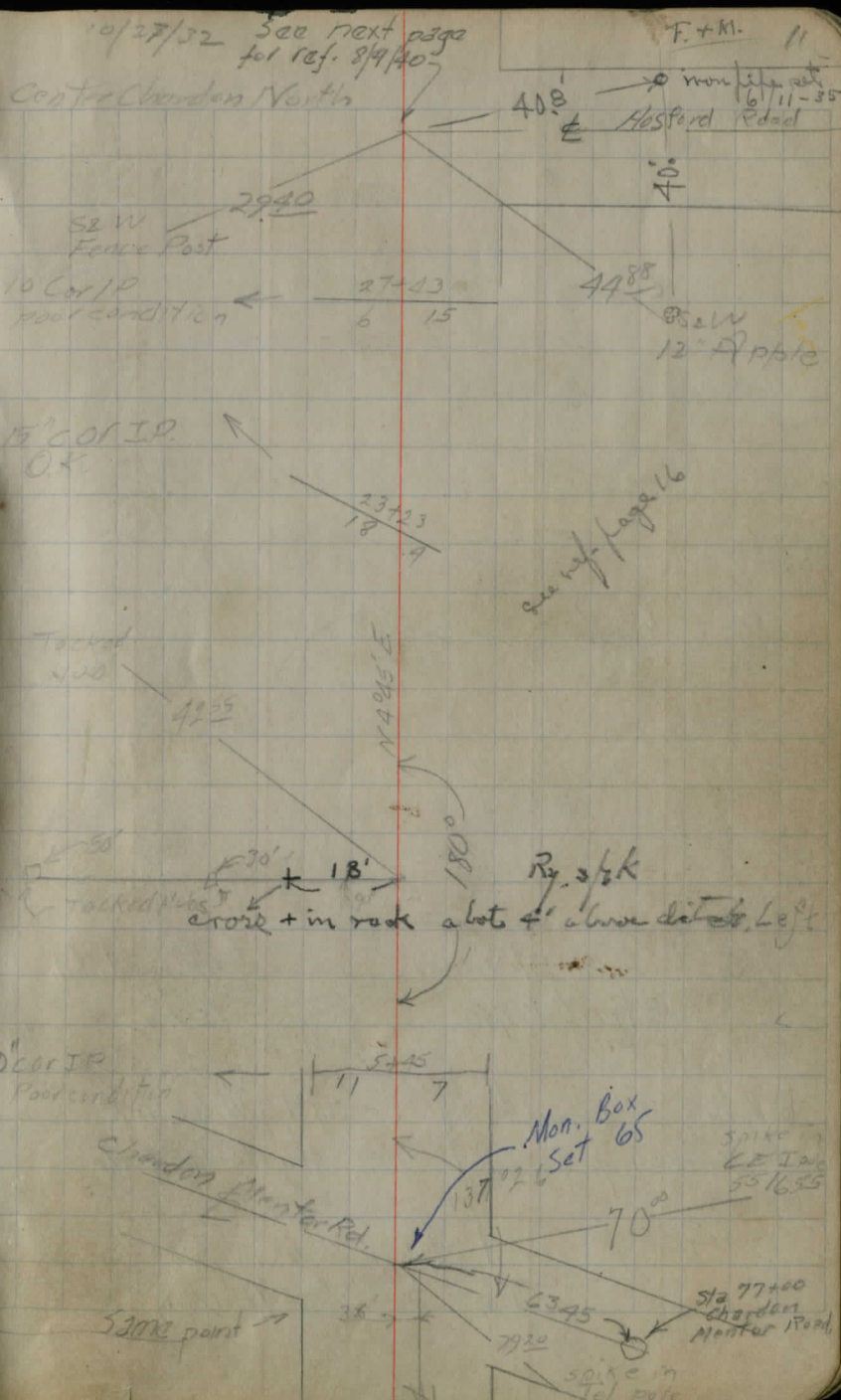
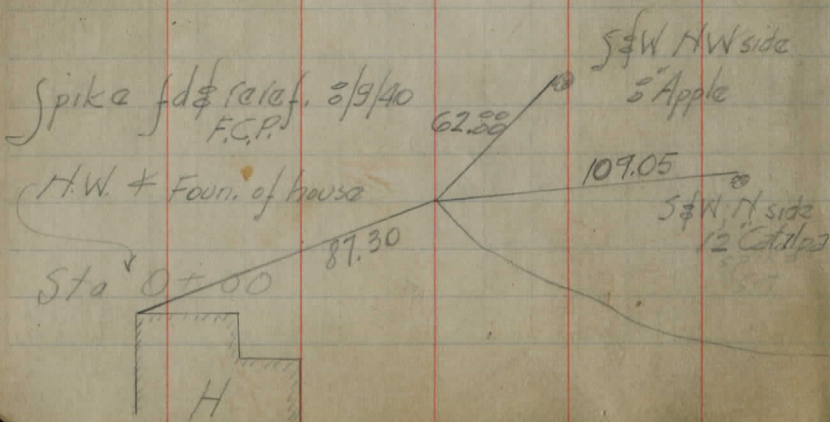
Location County Highway No 4
 Sta 27 + 65⁰⁰ E 30' on road
 Stafford Hill



11100⁰⁰

Sta 12 + 24⁷⁵

Def. 0° 00'



County Line

60' spike set

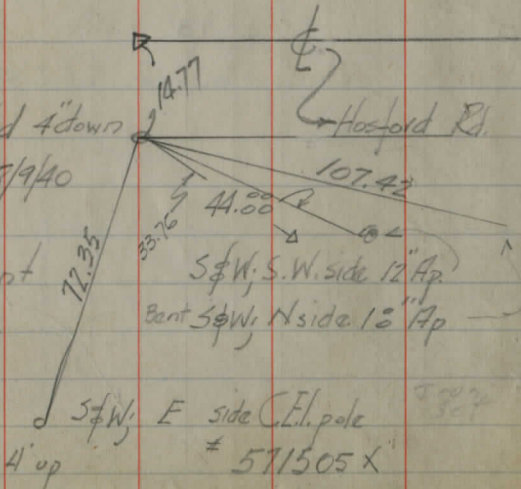
PI 600' ± South of C Line

Iron set

27+65" Pipe fd 4' down
16 ref. 8/9/40

Note: Same point
as preceding fg.

PI



740 270 2 RR L E
from map. W side 12
Center Road
Phelps & Parker.
Vol III P. 28811: 1897

Lake Co
Grays Co

Iron rod set in 12" base

2006'

Sec Pg. 39

Co Line Rd

See pg 19 approx profile



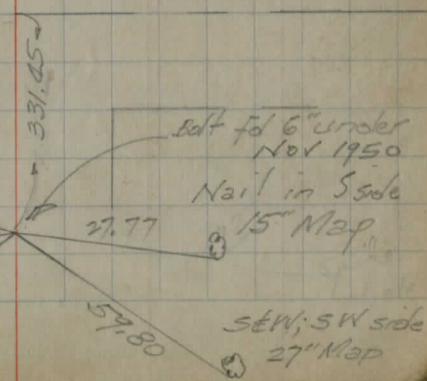
See pg. 19 approx profile

Clarks Crossing Rd

Spk in NE side
18" Buck

rod nail S side CEI # 571535

S.W. in SE side 18" Buck



Levels on CH No. 4 North of Ohio Gas Center

BM 6.79 1277.98 1271.19
 11.29 1288.99 0.28 1277.70

Sta 77 C.M. Road 2.48 2.49 1286.50

BM #1 3.42 1285.57

4.18 1282.20 10.97 1275.02

8.16 1290.19 0.17 1282.03

BM #2 4.48 1285.71

9+00 4.5 1285.7

10+00 4.0 1286.2

11+00 3.6 1286.6

Rock outcrop at 11+05

11+55 4.3 1285.9

11+92 4.6 1285.6

2.11 1286.31 5.99 1284.20

12+18 1.9 1284.4

12+20 2.1 1284.2

12+50 3.0 1283.3

13+00 8.5 1277.8

3.96 1277.20 13.07 1273.24

13+50 5.8 1271.4

W by NE Handwell 700' West X

2 spikes in W side 10' Elm 40' Lt & Sta 1+00

2 spikes E of 8' Locust 25' Rd Sta 8+50

25	16	12	8	3	10	12	13	16	30
22	33	45	42	36	38	42	37	32	25

30	18	14	7	5	8	13	15	30	
20	36	41	42	44	43	42	37	30	

30	17	13	8	8	11	15	18	30	
39	38	48	46	46	46	47	40	34	

30	14	11	8	14	15	16	25	11	6	8
09	12	19	19	15	17	14	07	14	13	14

30	14	11	8	14	15	16	25	11	6
09	11	21	17	15	18	15	02	13	18

30	14	8	8	10	13	16	30	20
20	27	42	38	29	31	35	26	25

30	23	11	9	6	8	9	12	14	16	33	30
58	61	70	75	80	82	82	80	87	83	60	58

30	19	9	7	5	12	14	18	27	30
09	11	50	63	57	58	61	45	07	-02

14+00	1277.20	12.0	1265.2
0.34	1264.51	13.03	1264.17
B.M. 3		4.35	1260.16
14+50		7.8	1256.7
0.43	1252.50	12.44	1252.07
15+00		4.7	1248.4
15+50		10.9	1241.6
1.21	1241.86	11.85	1240.65
16+00		8.2	1233.2
1.27	1230.38	12.75	1229.11
16+50		2.4	1228.0
17+00		7.5	1222.9
2.18	1220.09	12.47	1217.91
B.M. 4		4.56	1215.53
17+50		3.3	1216.8
11.0	1216.63		1215.53
18+00		5.5	1211.1
1.18	1204.79	13.03	1203.61
19+00		2.7	1202.1
20+00		10.6	1194.2
0.55	1192.73	12.91	1191.88

-27	13	12	9	4	5	11	13	16	19	20	26-
62	93	112	129	120	121	126	135	121	110	96	56

Spike Erect in Tulip 30' L & 5' W 14+50

30	26	15	12	8	7	11	14	15	30
40	45	70	79	71	80	68	78	73	41

30	55	17	13	8	10	18	20	25	30
39	35	38	44	41	34	40	38	41	00

25	20	15	9	5	9	12	30
116	114	125	108	119	109	125	123

-30	21	16	10	9	13	16	25
78	81	93	83	78	88	81	76

-27	33	19	18	17	12	15	17	21	30
07	39	46	37	33	29	36	29	21	-10

30	23	21	16	10	8	13	16	20	22-
78	86	95	88	80	79	87	87	69	48

Spike in W root 10' E in 30' R + Sta 18+02

-25	22	21	20	18	6	8	11	13	21-
78	34	43	34	34	34	50	27	27	9.2

-30	23	19	15	10	15	16	22	30	5
29	58	64	54	53	48	33	16	1.5	52

-25	32	20	16	15	8	11	12	17	21	27-
14	34	24	29	28	27	36	20	19	02	-0.5

30	17	18	16	15	14	9	8	11	13	19	30
57	102	113	99	99	106	103	104	116	107	92	94

9/17/30 (Ferry Rd) Brook Lane

Data for culvert on Picket brush

Road Chester Twp

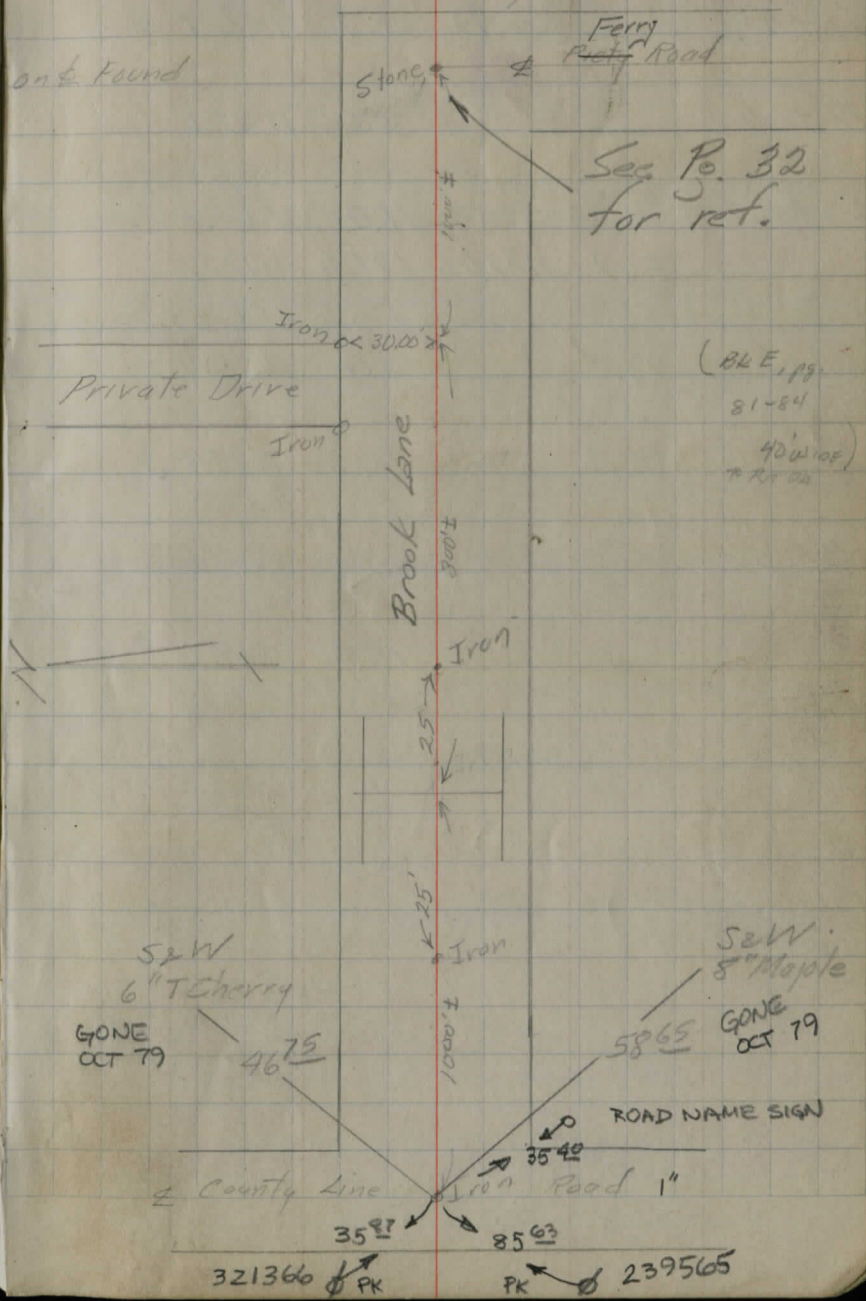
PI Picty Road & stone with hole drilled on & found

Iron Rod found on property line of private Road

Twin 3x6 stone Box culvert

POT County Line Road &

Iron found



21+00 119243 5.7 1186.7

22+00 8.8 1183.6

23+00 11.4 1181.0

269 118206 1306 1179.37

Calc.

24+00 5.2 1176.9

25+00 10.3 1171.9

BM 5 438 1177.68

26 16.8 1165.3

27

$\frac{25}{38} \frac{278}{50} \frac{1275}{62} \frac{1471}{53} \frac{10}{60} \frac{7}{55} \frac{8}{55} \frac{12}{54} \frac{21}{55} \frac{25}{48}$

$\frac{30}{25} \frac{10}{23} \frac{6}{88} \frac{8}{88} \frac{10}{96} \frac{25}{100}$

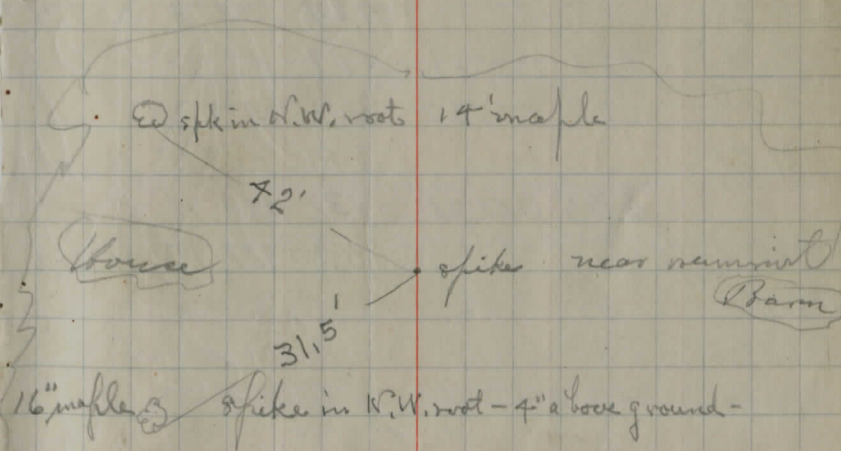
$\frac{30}{118} \frac{22}{113} \frac{15}{119} \frac{11}{122} \frac{10}{112} \frac{3-5}{107} \frac{6}{126} \frac{2}{114} \frac{18}{106} \frac{20}{102}$

$\frac{41}{20} \frac{41}{36}$

$\frac{23}{30} \frac{10}{67} \frac{17}{54} \frac{13}{46} \frac{9}{29} \frac{12}{17} \frac{25}{13}$

$\frac{22}{80} \frac{13-17}{118} \frac{16}{105} \frac{18}{98} \frac{7}{124} \frac{3}{104} \frac{5}{108} \frac{6}{100} \frac{7}{89} \frac{14}{70} \frac{15}{61}$

Top Sand 3x3 Boulder 35ft + 2 5/8 20+80



Ref. 6/11-35, F. x Maple

118206

1275 119212 2.69 117937

1305 120494 0.23 119189

13.13 1216.75 1.32 1203.62

BM 4 1.22 121553 121553

12.97 1229.15 0.17 121658

12.35 1241.32 0.18 1228.97

13.11 125373 0.70 1240.62

10.94 126299 1.68 125205

B 4 3 2.84 126015 1260.16

1267 127562 0.04 1262.95

13.19 1286.54 0.27 1275.35

3.36 129000 1.90 1286.64

B 4 2 4.27 128573 1285.71

4.52 128251 12.01 1277.99

620. 1286.30 0.91 1282.10

BM #1 2.81 128549 1285.51

0.35 1281.33 7.32 1280.98

Had wall in CM Post 10.20 1271.13 1271.19

Devison - Fiedler - 4-14-33 - (P.W.)

Warner + cloudy
STAFFORD Hill CH #4

WD

ELow.

1260.16

B 11/3

+ 0.15 1260.31

15

11.93 1248.38

14 + 50

7.52 1255.99

T P

-0.60

+ 12.60 1278.31

1259.71

14

12.00 1260.31

13 + 50

6.15 1266.16

13

0.85 1271.96

T.P.

-0.20

+ 11.80 1288.91

1278.11

12 + 50

7.82 1276.09

12

4.40 1279.51

11 + 50

0.61 1283.80

T P

-0.10

+ 6.23 1290.04

1283.81

11

4.70 1285.34

10 + 50

3.87 1286.17

10

4.13 1285.81

2 B.M. not found

M.L. Bailey - Robinson - Diederich

Low spot in Chardon Auburn Rd ± 800' N
of Clark Station Rd.

7.12	F.L. (E end) 12" cov	
10/21/47	4.68	£ road
	-6.68	F.L. West 12" cov
FR3	-5.1	100' N. on £
S. Merritt	-4.9	200' N. on £
	-7.5	100' N. E. outlet
	-4.6	100' S. on £
	-5.8	" " " " W. Ditch
	-5.75	" " " " E. "
	4.4	200 " " " £
	5.25	" " " " W. Ditch
	5.3	" " " " E. "
	3.5	300 " " " £
	4.7	" " " " W. ditch
	4.25	" " " " E. "
	2.3	400 " " " £
	3.6	" " " " W. Ditch
	3.2	" " " " E. "

-4.35	= £ at 100' N. of Jonesek's N —
4.45	= £ " 175' " " " = drive to W.
5.75	= 12" down pipe (S. end) on W ↑
5.75	= " " " (N ") " "
4.50	= £ at 200' N. of Jonesek's N —
4.85	= £ " 300' " " " " " "
5.9	= W. ditch " " " " " " "
5.15	= £ 400' " " " " " "
6.45	= W ditch " " " " " "
5.65	= £ 500' " " " " " "
7.2	= W ditch " " " " " "
6.9	= £ 600' " " " " " "
-4.25	= 200 W of £ & 25' N. of Jonesek's N —
4.8	= 300' " " " " " "

Chardon Auburn Rd line
± 1500' S of Lake Rd

10/21/47	-3.6	£ N. line Jonesek
	-4.9	W. ditch " "
	4.25	75' N. on £
	5.7	" " " " W. ditch
	6.05	" " " " E. "
	6.05	100' E. in outlet
	6.15	200' E. " "
	5.7	300' " " " "

11/29/33

Goodrich, R
Rhodes, A C. Bliss

Levels on Co. H. No 4.

BM [#] 2	4.72	1290.43		1285.71	
9			4.5	85.9	
10			4.0	86.4	
+50			3.7	86.7	
11			4.5	85.9	
+50			6.6	83.8	
12			10.4	80.0	
+50			14.0	76.4	
T.P	0.15	1275.90	14.68	1275.75	
13			4.0	71.7	
+50			9.2	66.7	
	1.75	1263.51	14.14	1261.76	
14			2.4	61.1	
+50			7.5	56.0	
BM [#] 3	3.38	1263.54	3.38	1260.13	1260.16
15	0.88	1250.80	13.62	1249.92	
15			2.3	48.5	

20

2 spikes in E root 8^o Locust 25' Rt. & Sta. 8+50
$$\begin{array}{cccc} \frac{25}{4.1} & \frac{16}{4.4} & \frac{14}{5.8} & \frac{10}{4.9} \\ \frac{10}{5.4} & \frac{13}{6.0} & \frac{18}{4.2} & \frac{28}{3.6} \end{array}$$

$$\begin{array}{cccc} \frac{25}{4.3} & \frac{16}{4.4} & \frac{14}{5.3} & \frac{11}{4.6} \\ \frac{11}{4.6} & \frac{14}{5.2} & \frac{15}{4.0} & \frac{25}{4.4} \end{array}$$

$$\begin{array}{cccc} \frac{25}{3.5} & \frac{16}{3.9} & \frac{15}{5.2} & \frac{10}{4.3} \\ \frac{11}{4.2} & \frac{14}{4.6} & \frac{16}{3.5} & \frac{25}{3.4} \end{array}$$

$$\begin{array}{cccc} \frac{25}{2.9} & \frac{17}{3.5} & \frac{14}{4.9} & \frac{11}{4.9} \\ \frac{12}{4.5} & \frac{15}{4.7} & \frac{17}{3.3} & \frac{25}{3.2} \end{array}$$

$$\begin{array}{cccc} \frac{14}{3.4} & \frac{17}{2.6} & \frac{13}{7.1} & \frac{12}{6.7} \\ \frac{15}{7.6} & \frac{19}{3.8} & \frac{25}{3.5} & \end{array}$$

$$\begin{array}{cc} \frac{12}{12.2} & \frac{75}{11.2} \\ \frac{15}{10.3} & \frac{16}{11.2} \end{array}$$

$$\begin{array}{cc} \frac{15}{15.3} & \frac{13}{14.1} \\ \frac{13}{14.3} & \frac{16}{15.7} \end{array}$$

$$\begin{array}{cc} \frac{15}{5.0} & \frac{13}{4.2} \\ \frac{15}{4.0} & \frac{17}{5.1} \end{array}$$

$$\begin{array}{cc} \frac{16}{10.4} & \frac{13}{9.4} \\ \frac{12}{9.0} & \frac{16}{10.3} \end{array}$$

$$\begin{array}{cc} \frac{17}{3.7} & \frac{15}{2.6} \\ \frac{14}{2.6} & \frac{17}{3.9} \end{array}$$

$$\begin{array}{cc} \frac{15}{7.9} & \frac{14}{7.6} \\ \frac{13}{7.8} & \frac{15}{8.5} \end{array}$$

$$\begin{array}{ccc} \frac{17}{2.7} & \frac{16}{3.4} & \frac{14}{2.8} \\ \frac{17}{2.1} & \frac{19}{3.8} & \frac{20}{2.7} \end{array}$$

1250.80

15+50 9.0 41.8

16 14.9 35.9

0.18 1234.69 16.29 1234.51

+50 4.4 30.3

17 9.6 25.1

0.79 120.73 14.75 1219.94

+50 1.0 19.7

18 5.7 15.0

BM 5.15 120.68 5.15 1215.58 1215.53

+50 10.4 10.3

1.86 1207.28 15.26 1205.42

19 1.6 05.7

+50 6.2 01.1

20 9.9 97.4

11.50 1216.92 1.06 1205.42

1.38 1215.54

19 16 13
10.5 11.3 10.0

17 18
9.9 10.3

22 14
78.5 15.7

17 21
16.3 16.4

22 14
8.9 5.1

14 17
5.4 6.2

22 13
13.1 10.4

15 18
10.3 11.8

24 15
4.7 1.3

11 17
1.4 2.3

22 12
9.8 6.5

10 17
6.1 7.1

23 11
13.7 10.9

12 17
10.9 12.1

20 14
5.1 2.6

15 19
2.5 3.5

19 12
8.2 6.3

14 19
6.8 8.4

17 14
12.3 10.6

15 19
10.8 11.5

12/1/33

R. Goodrich
C Bliss

BM #2	5.68	1291.39	1285.71	
9			5.06	1286.33 4.06
+50			4.89	1286.50 4.89
+75			4.92	1286.47 4.92
10			5.15	1286.24 4.65
+25			5.61	1285.78 4.11
+50			6.28	1285.11 3.78
+75			7.17	1284.22 3.67
11 +0			8.26	1283.13 3.76
	3.02	1288.03	6.38	1285.01
+25			6.22	1284.81 0.22
+50			7.75	1280.28 4.25
+75			9.50	1278.53
12			11.46	1276.57

22

Stakes are graded to \pm Grade.Stakes Set 25 Rt \pm

C 1.0

C 0.0

C 0.0

C 0.5

C 1.5

C 2.5

C 3.5

C 4.5

C 6.0

Lt

Rt

Marked on

C 3.5

C 3.5

Rock

5.50

C 4.0

C 4.0

5.50

7.96

C 3.5

C 3.5

7.96

1288.03

12 + 25 13.64 1274.39

+50 16.03 1272.00

0.84 1274.65 14.22 1273.81

13 7.65 1267.00

+50 12.65 1262.00

14 17.65 1257.00

STK

+50 22.65 1252.00 14.65

2.10 1260.65 16.10 1258.55

15 0.48 1260.17 1260.16

15 13.65 1247.00 11.65

0.27 1244.87 16.05 1244.60

+50 2.87 1242.00 3.87

16 7.87 1237.00 9.87

+50 12.87 1232.00 14.87

0.91 1230.95 14.83 1230.04

17 3.95 1227.00 4.95

+50 8.95 1222.00 10.45

23

LT. RT

8.64 C5.0 C5.0 8.64

11.53 C4.5 C4.5 11.53

2.65 C5.0 C5.0 2.65

7.65 C5.0 C5.0 7.65

12.15 C5.5 C5.5 12.15

C8.0 Marked on Stake 25' RT. E

C2.0

F1.0

F2.0

F2.0

F1.0

F1.5

1230.75

18+00 13.95 1217.00 15.45

15.41 1215.54

F1.5

+50 0.68 1215.39 16.24 1214.71

+50 3.39 1212.00 4.39

F1.0

19 8.39 1207.00 9.89

F1.5

+50 13.20 1202.19 15.70

F2.5

20

Sec. B

Cuyahoga-Geauga County Line Road
Sta 9+69.2

Spike
Found

Note: Sidestakes are set 25' RT or East

Sta 6+00 POT

Pipe
Set

Sta 0+00 ± Wilson Mills Road

Spike
Set

8/2/74 Rich-
Perry

26

Wilson Mills Road North

P.L. pipe ← 22.25 → 22.6 → Spike

S&W
8" Maple

56.81

57.38

S&W
10" Elm

N 45° 30' E

X cut in center
Wind N Headwall

X cut NE of
N Headwall

Spike Spot
15" Maple

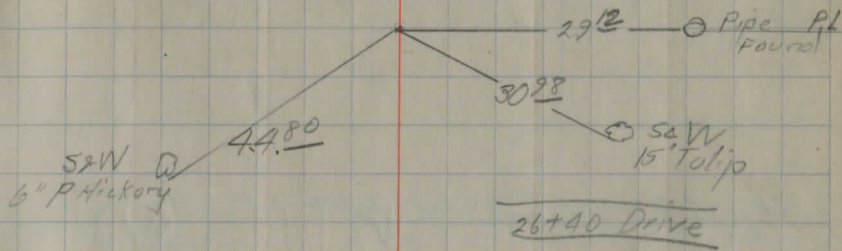
± Brigham Road

Wilson Mills Rd.

} 7.33'

Sta 29+55³⁰ POT

Pipe Found



Sta 23+85

PL pipe ~~OK~~ 28.35 →

drainage ← 23+25 drainage →
 No culvert
 drainage ditch required
 both ways

Drive 18+40

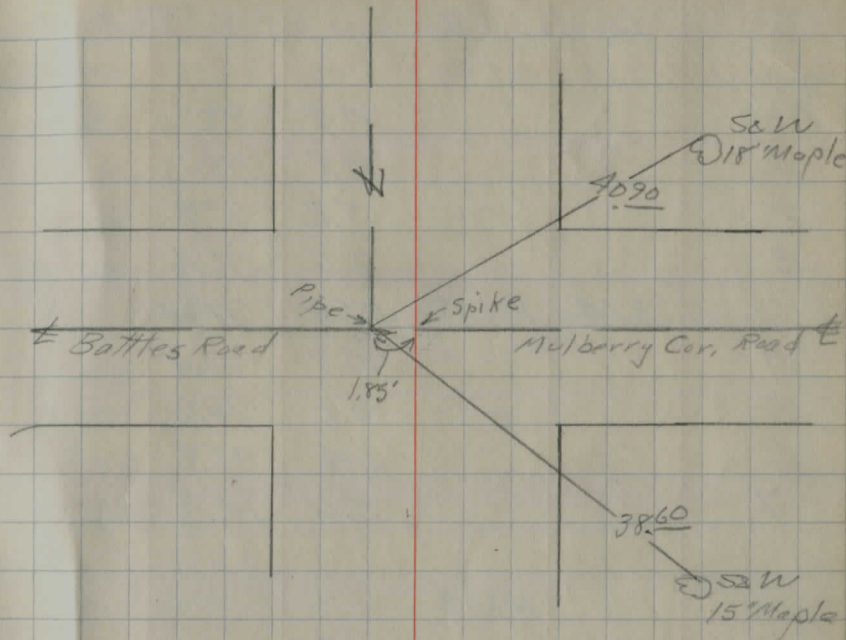
16+50 Drive

Sta 11+30

← 23.00 → ○ pipe PL

Sta 48+20.28 ± Battles Road Spike Set

.91 miles.



12" CIP in good condition Fl Rt

44+0A
10 9



40+10 Drive

pipe D ← 28.3 →

Sta 32+02

Levels on Drainage Ditch Sect B

Top boulder	290	102.90		100.00
0+00			4.7	98.2
1			4.8	98.1
2			5.2	97.7
3			6.5	96.4
	3.74	101.08	5.56	97.34
4			4.7	96.4
5			5.1	96.0
6			5.4	95.7
7			5.6	95.5

101.08

6			5.73	95.35	3.73
TP	5.12	102.46		97.34	
4			6.41	96.05	4.41
2			5.71	96.75	2.71
0					

to East

20.91 ±	Sta 23 + 30
97.45	↑
97.10	
96.75	
96.40	0.30%
96.05	
95.70	
95.35	
95.00	↓

$$\begin{array}{r} 35 \\ 7 \overline{) 25} \\ \underline{21} \\ 40 \\ \underline{35} \\ 5 \end{array}$$

$$\begin{array}{r} 33 \\ 2 \overline{) 66} \\ \underline{66} \\ 0 \end{array}$$

- C 2.0
- C 2.0
- C 3.0
- C 3.0

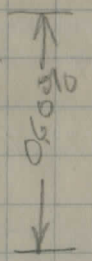
Levelson Drainage Ditch to West

S/O 23+25

Top boulder 225 10225 100.00

0	3.8	97.4
1	4.8	97.4
2	5.2	97.0
3	5.9	96.3
4	6.9	95.3

97.40
96.80
96.20
95.60
95.00

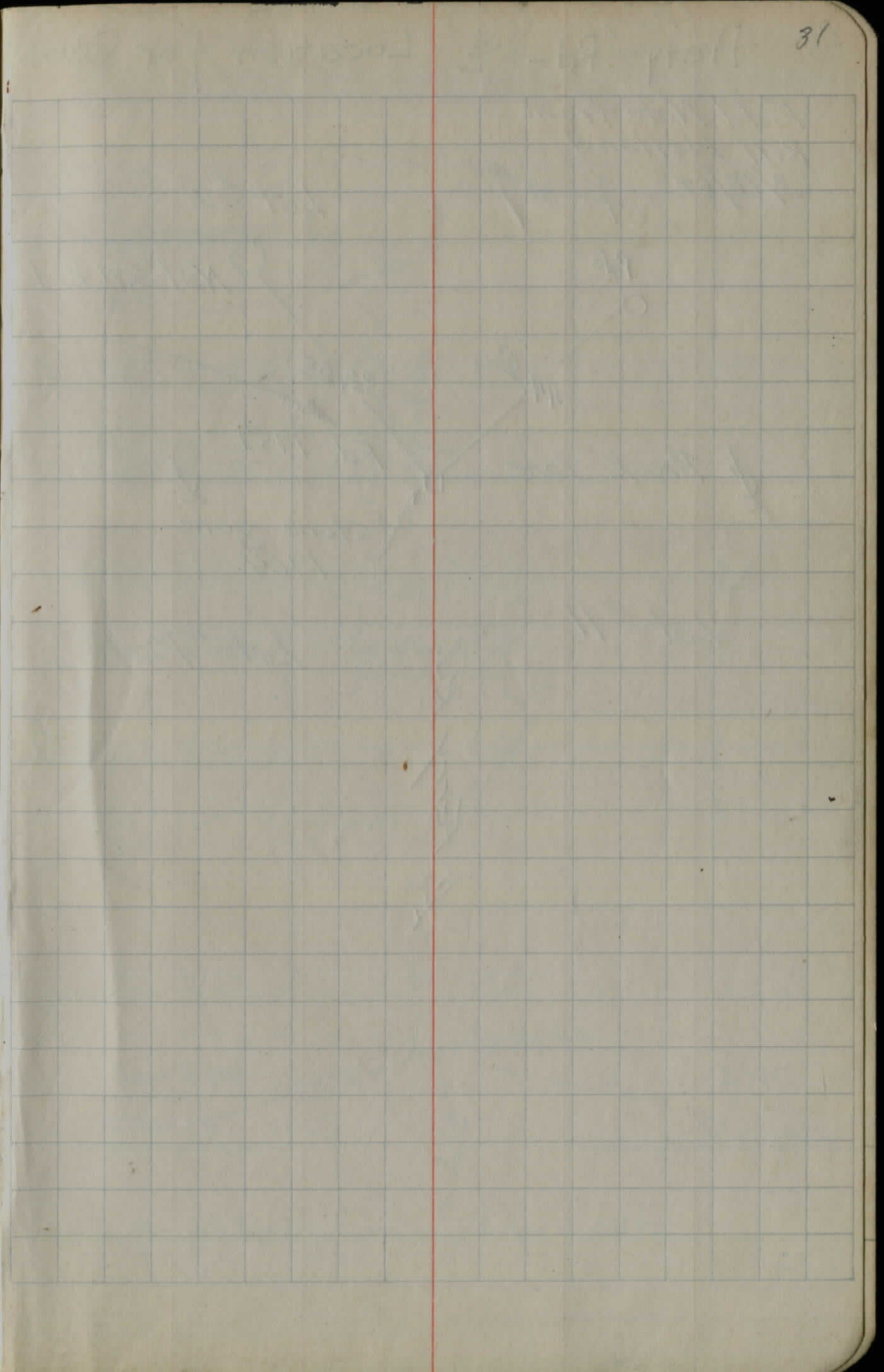
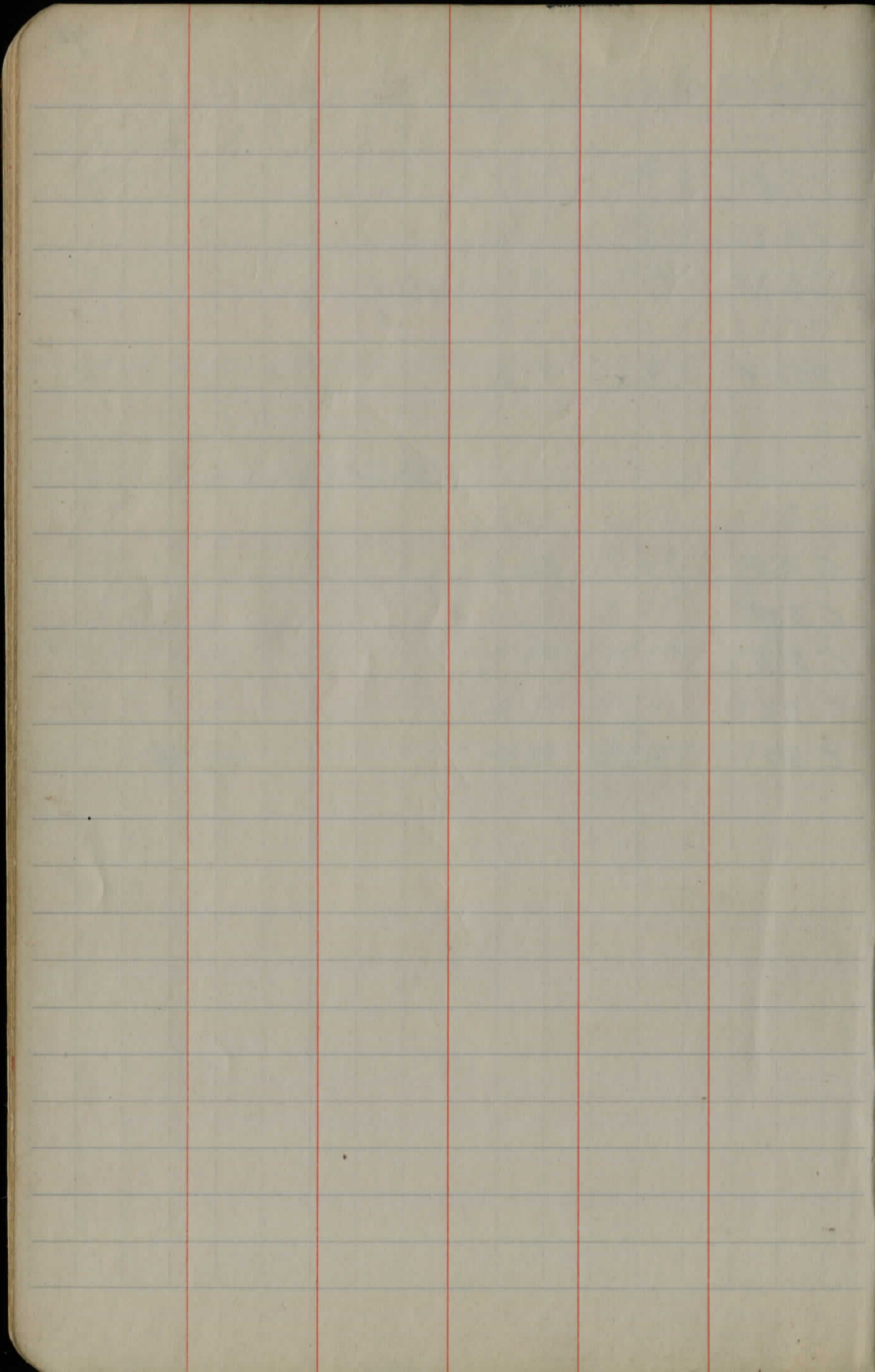


4/25
.6

10225

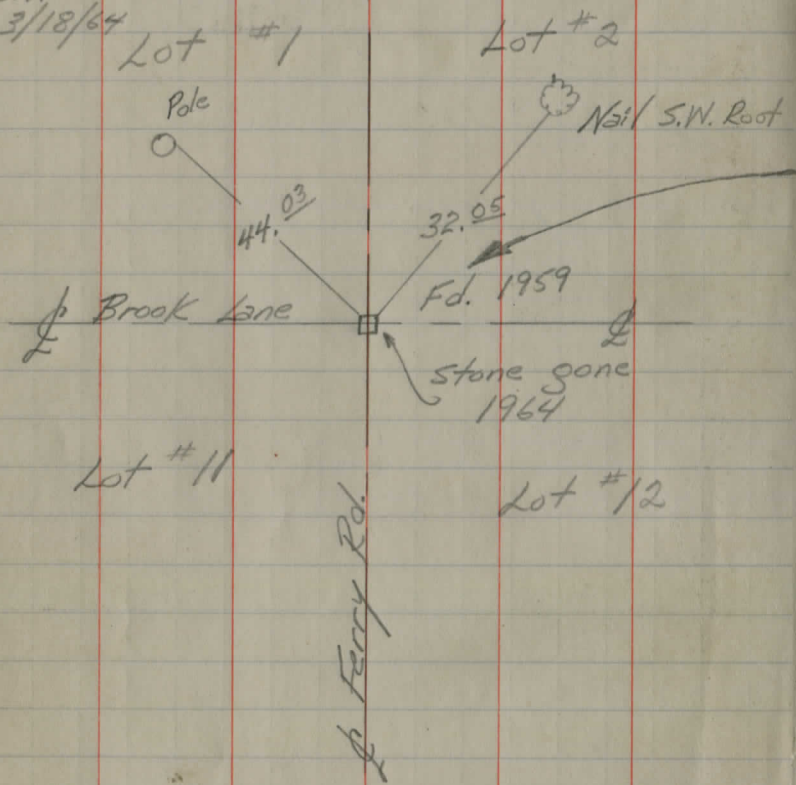
4	7.25	95.00	5.25
3	6.65	95.60	3.15
2	6.05	96.20	3.05
1	5.45	96.80	2.95
0	4.85	97.40	1.85
0 on East line	4.80	97.45	1.80

C 2.0
C 3.5
C 3.0
C 2.5
C 3.0
C 3.0

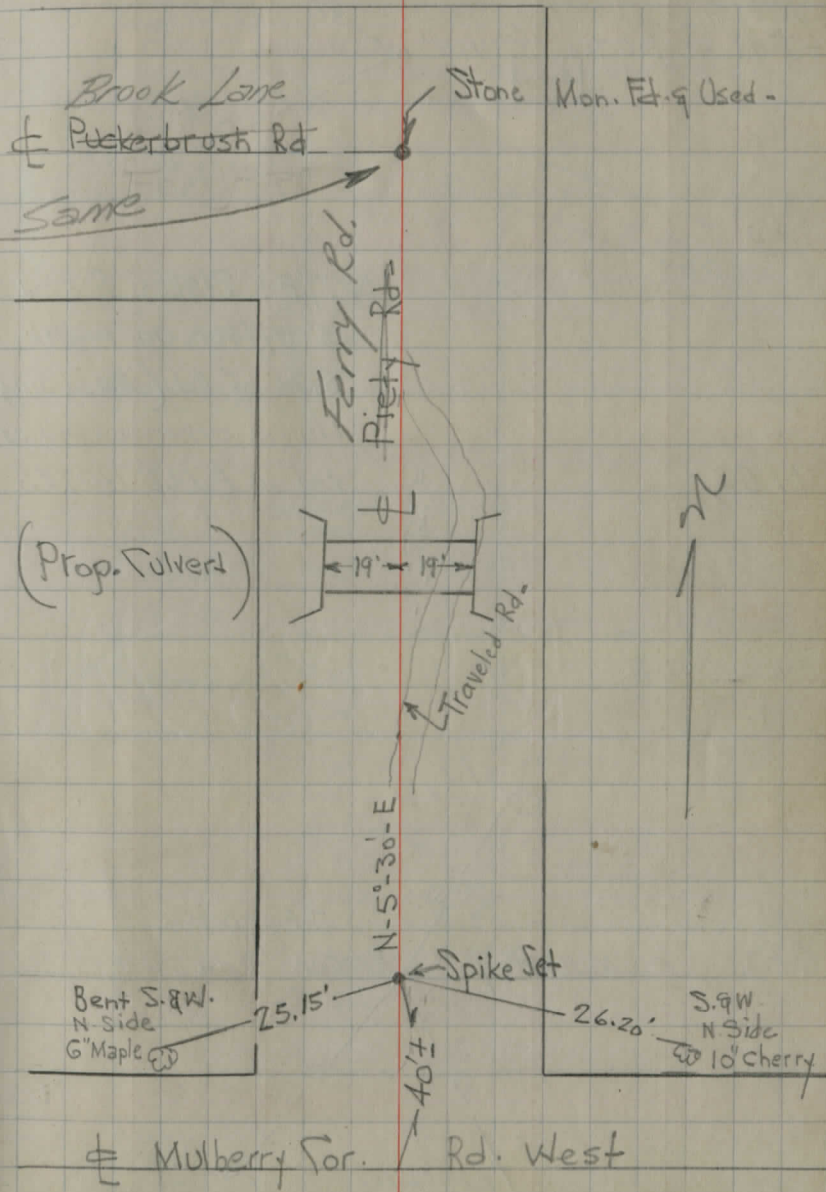


(Ferry)
Piety Rd - \perp Location for Culvert

Field Note from
Bill Holland
3/18/64



Aug. 20, 1935



14
13
12+50
12
11
10+15
10
9
8
7
6
5
4
3

N-5°-30'-E

4'-6" x 5' x 38' New Conc. Box Culvert

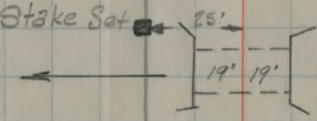
12+98 Fence ↘

Stake Set ← 25'

12+45 Fence ↘

Stake Set ← 25' → 25' → Stake Set

Stake Set ←

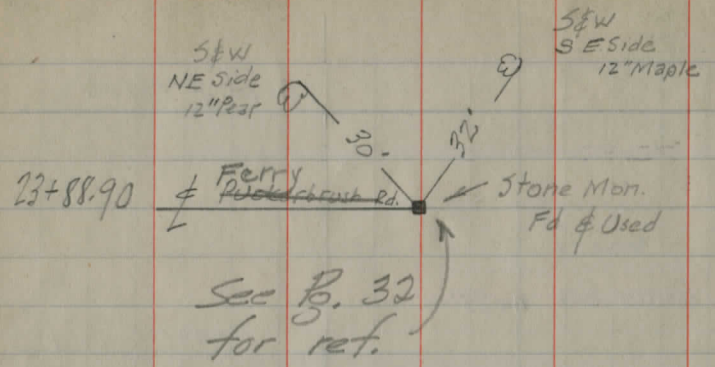


4'-6" x 5' x 38' Conc. Box Culv. (NEW)

↘ 8+90 (old Fence Line)

14+30 E Drive

6+37 W. Fence ↘



23

22

21

20

19+77 12" x 32" (CIP & Cor. I.P. Fair Cond.)

18" Pipe Reg'd.

19

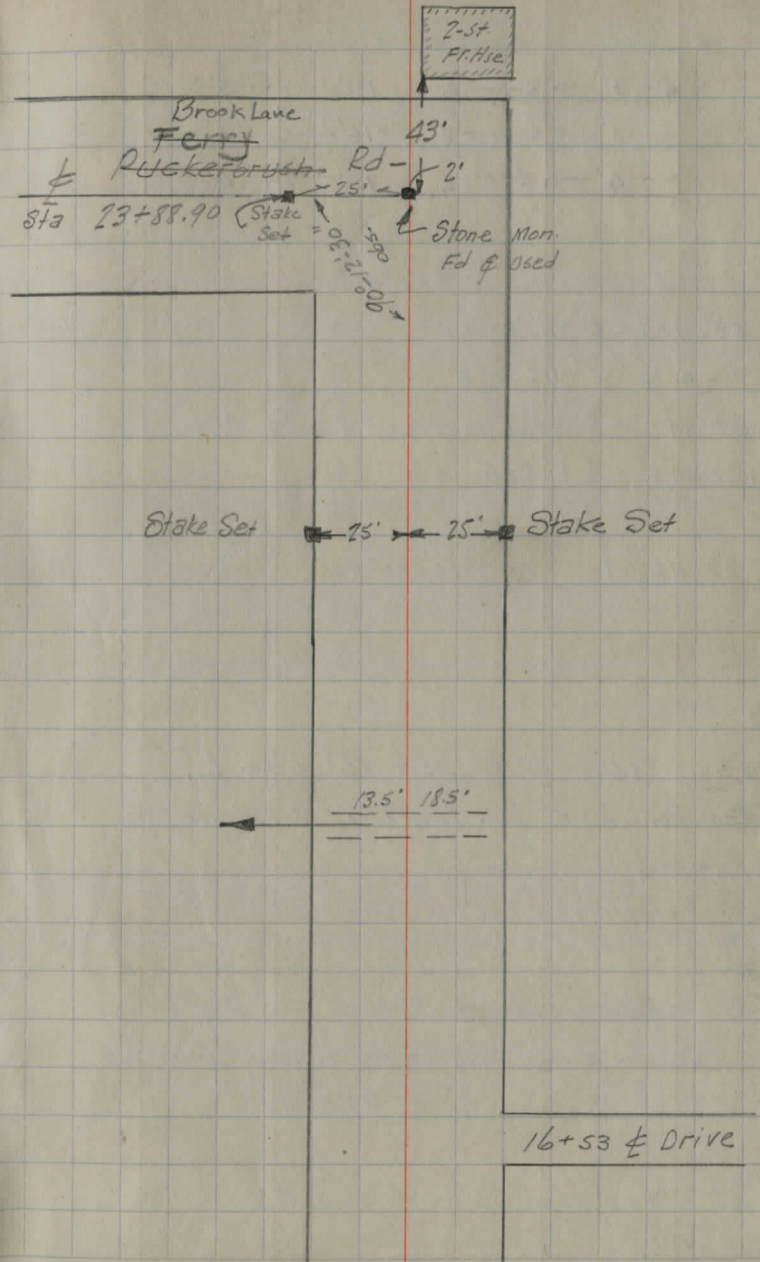
18

17

16

15

N-5°-30'-E



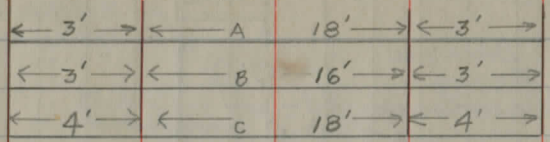
Stake Set

25'

Stake Set

13.5'

18.5'



BEGIN 0+26.5 = N Edge Pave of "8" AT "A"

58+11.05 = & Towing Rd

96+60.38 = & U.S. R'd G

182+01 = S. EDGE PAVE OF "5" AT "A"

182+4.8 = I.T. #4 & 5

139+46.67 Δ = 0°-16'-30" RT

7-25-50

SIDE STAKES FOR MA SET 15' from E.

Center line 30' 4" from Point Stone Nat. H. Line

Cut Brown from RT6 to "5"

SIDE STAKED FROM RT6 to 120+00

7-26-50 STAKED 120+00 to 180+00

LINE NEAR W EDGE BASE AT 126 to 132; 164 to 166

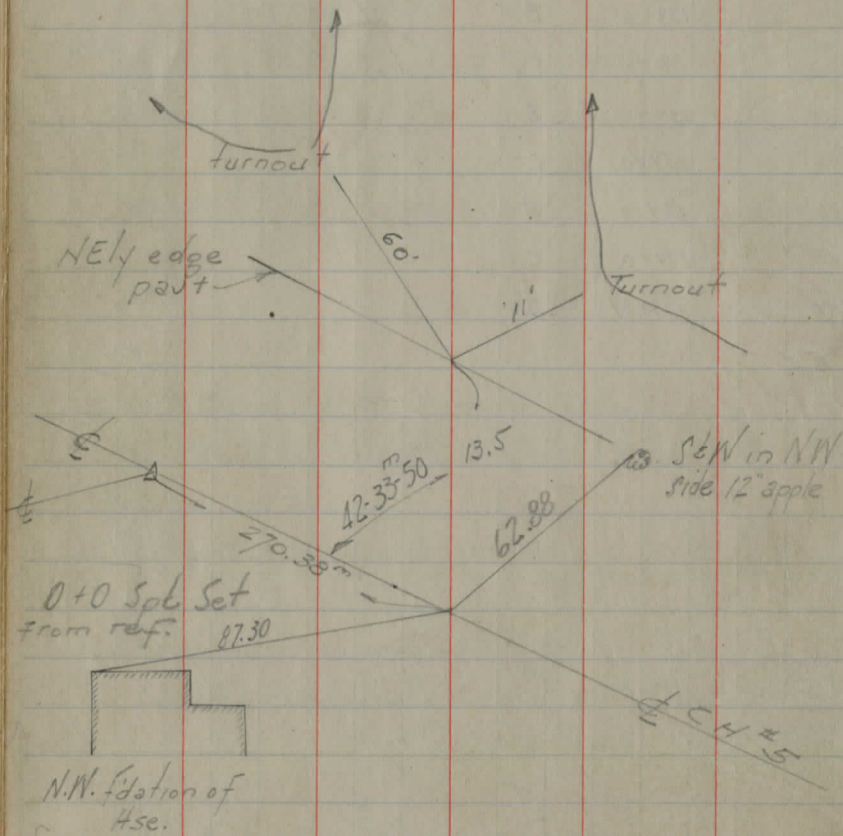
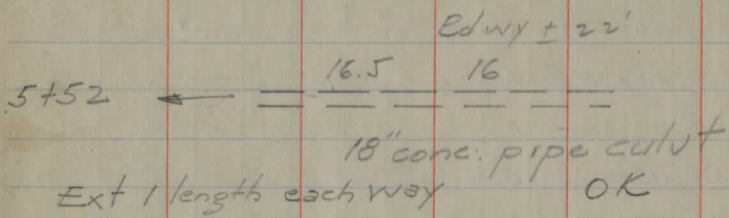
" " E " " " 147 to 149

7-31-50 MIX & Lay 158+00 to ± 182

0+26.5	-	42+0	A
43+0	-	46+0	C
47+0	-	58+02	A
58+18	-	96+50	A
96+70	-	112+0	B
119+00	-	122+0	C
123+0	-	138+0	B
139+0	-	140+0	C
141+0	-	154+0	B
155+0	-	158+0	C
159+0		169+0	B
170+0		171+0	C
172+0		182+01	B

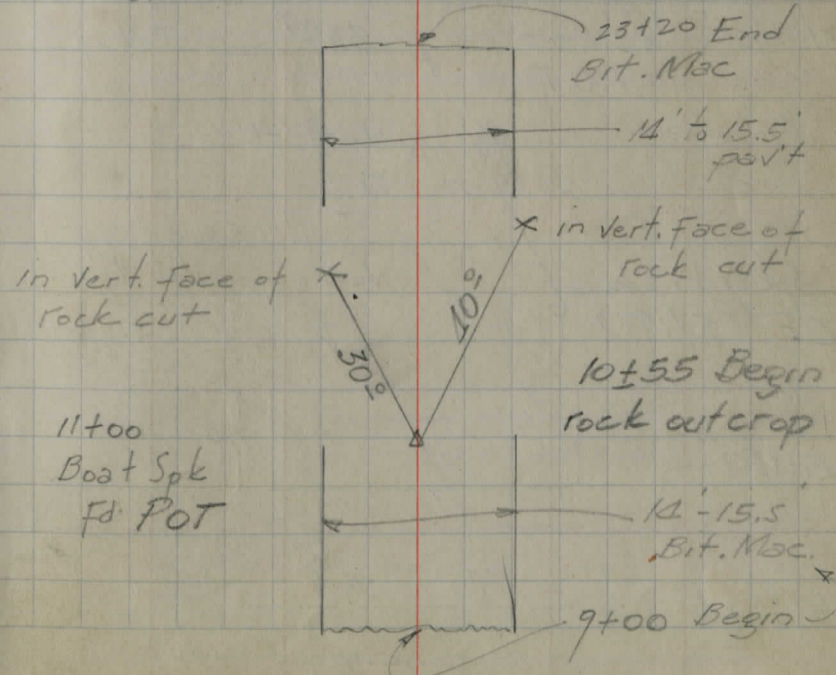
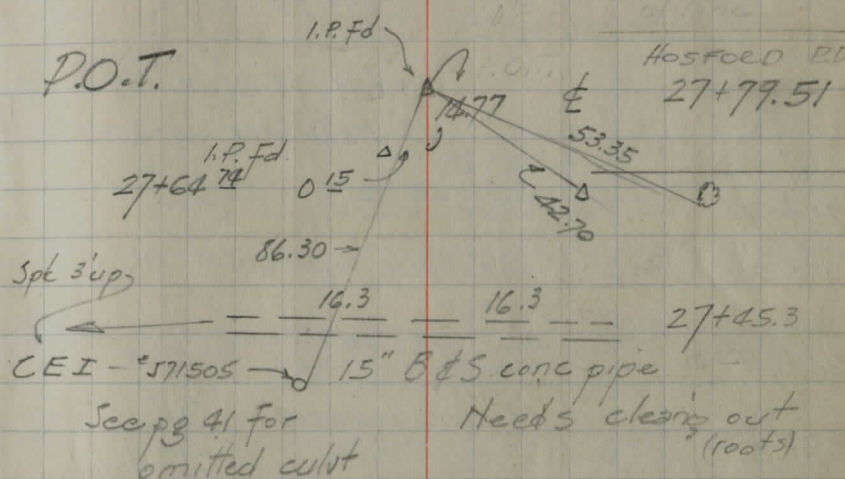
March 1951
Pom - Maynard - Lewis

AUBURN RD



1- 1103.20
2- 1820.35

#4 - STU



78+54.85

1. pin fd See ref. pg 12

74+76

12.5 → 21

15" conc pipe culut OK

64+67

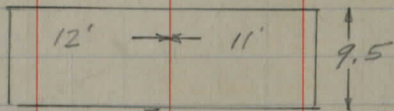
14.5 → 19

18" conc. pipe culut OK

51+73.25 3/4" I.P. set P.O.T

Spk NW side CE I # 571519

43+65.7



36+97.4

16.7 → 16.8

15" conc. pipe culut OK

(Insufficient at high H₂O (per Jackson))

179-44

359-28

Big rock partially blocks inlet

105+70

Verrick I.P. Δ

Spk N side 15" Apple

23+27.20 bolt fd

CLARK RD

SEW; E side 20" Map

12" conc pipe culut OK

See pg 50

13 → 21

OK

SEW; E side 20" Map

CLARK RD

Bolt set

89-53.30

179-47

13.7

28.8

Bent I.P. Δ

Spk S side CE I N of Copperman drive # 395708

27.45

32.0

Spk N side 15" Apple

27.25

103+13

11.3

13.2

2.66 span x ± 2' Stone culut.

96+00 P.O.T

21.76

90+49.7

19.5

88+95

12" conc. pipe culut relay (lower FL?)

65.60

61.82

24" Map

21

OK

12" conc pipe culut

24" Map

SDW W side

SDW NE side

12" conc. pipe culut relay (lower FL?)

88+95

19.5

90+49.7

CE I N of Copperman drive # 395708

Spk S side

21.76

96+00 P.O.T

Spk S side 10" M.

IF new culut skew SW-NE

30.9V Δ I.P. TRB.?

9.5

11.5

2.66 span x ± 2' Stone culut.

clean outlet ± 100'

IF new culut skew SW-NE

30.9V Δ I.P. TRB.?

9.5

11.5

2.66 span x ± 2' Stone culut.

Spk S side 10" M.

Spk S side 15" Apple

IF new culut skew SW-NE

30.9V Δ I.P. TRB.?

9.5

11.5

2.66 span x ± 2' Stone culut.

81+30

Sta. 81+86.5

Bolt set

12" conc. pipe culut relay (lower FL?)

88+95

19.5

90+49.7

CE I N of Copperman drive # 395708

Spk S side

21.76

96+00 P.O.T

Spk S side 10" M.

IF new culut skew SW-NE

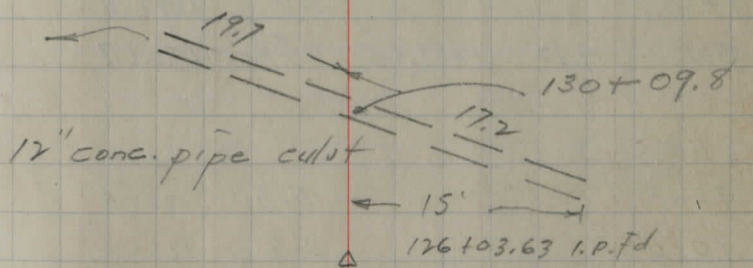
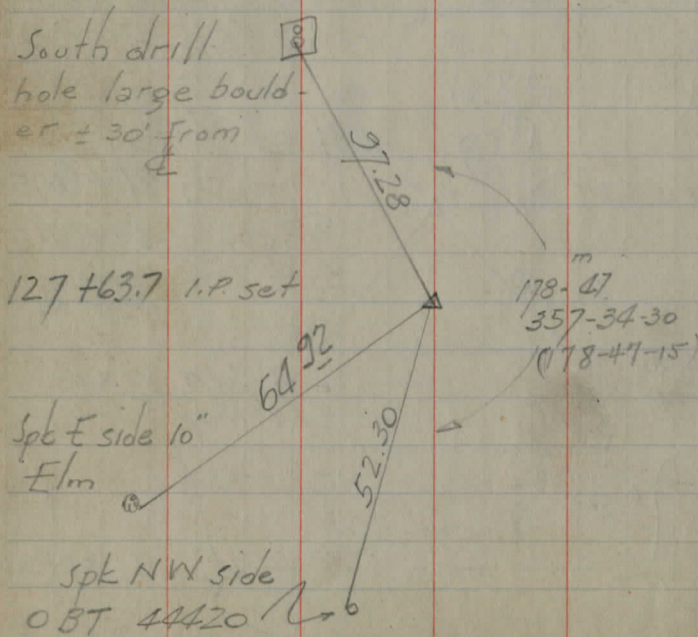
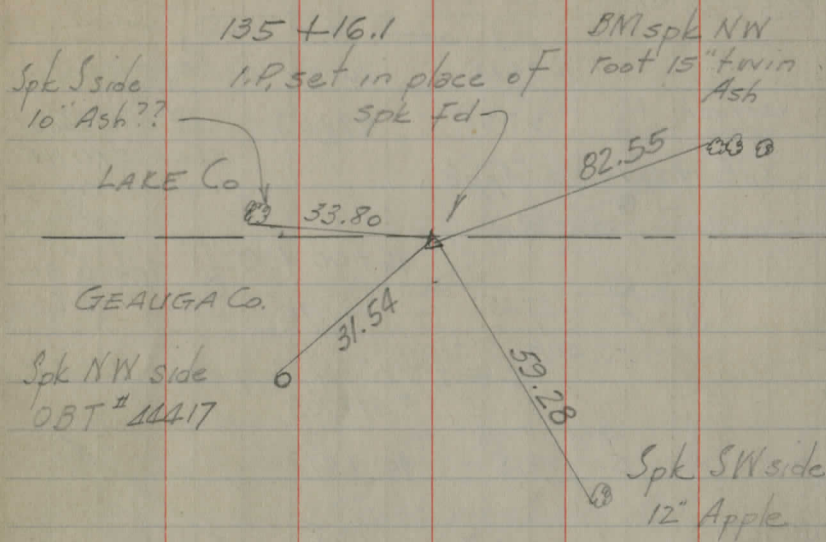
30.9V Δ I.P. TRB.?

9.5

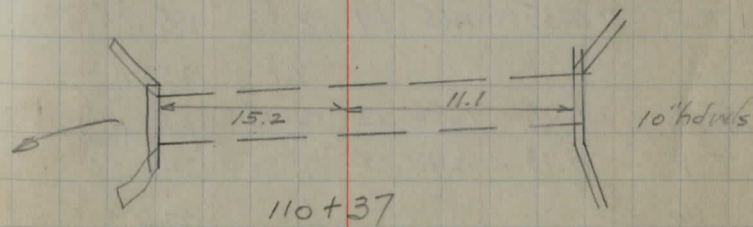
11.5

2.66 span x ± 2' Stone culut.

38



116 + 88 29.95 I.P. FRZ



4.5 spm x 3.54 + Stone walls
conc slab & hdwls & wings OK

MARCH 27th 1951 + H 1
 CENTER CHARDON NORTH ON AUBURN ROAD

BM	3.09	1287.00		1283.91
0+0			2.70	1284.3
1+0			4.7	1282.3
2+0			6.2	1280.8
T.P.	2.50	1281.20	8.30	1278.70
4+0				
5+			culvt	
6+0			4.6	1276.6
7+0			3.5	1277.7
T.P.	9.17	1289.84	0.53	1280.67
8+0				
9+0			5.3	1284.5
10+0			4.8	1285.0
11+0			8.0	1281.8
T.P.	1.09	1277.97	12.96	1276.88
12+0				
T.P.	0.35	1265.49	12.83	1265.14
14			9.1	1256.4
T.P.	1.08	1254.12	12.45	1253.04
T.P.	0.13	1241.39	12.86	1241.26
16			5.2	1236.2

POMEROY-LEWIS-TURBIE-MAYNARD

40

Spk S root 20" Elm NW 1/4 of #4 & #5

76.1	76.6	76.3	76.6	77.1	1277.1	76.5	75.8	77.2	77.1
5.1	4.6	4.9	4.6	4.1	4.1	4.7	5.4	4.0	4.1
300	16.0	15.0	11.5	5.0		10.0	12.0	15.0	30.0

1271.8	73.2	76.4	1273.2
9.4	8.0	4.8	8.0
100'	FL		FL

1281.8 81.5 82.8

(8)

8.3

(7)

0 = edge trad rd

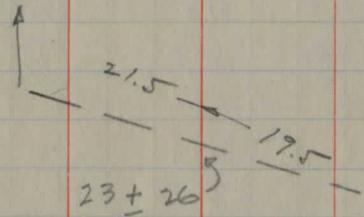
16' left up
 15' ditch
 16' part
 1275.4
 2.6
 15' ditch
 16' vert up

56.4

	+	H I	-	E
		1241.39		
T.P.	0.58	1229.71	12.26	1229.13
17			3.7	1226.0
T.P.	1.04	1217.80	12.95	1216.76
18			2.1	1215.7
BM set			3.22	1214.58
T.P.	0.40	1206.07	12.18	1205.62
20			8.0	1198.
T.P.	0.77	1193.83	12.96	1193.06
22				

T.P. 1.60 1182.68 12.75 1181.08

23+70 end point 2.7 1180.0



15" Conc pipe culvt OK

24+0			6.1	1176.6
T.P.	5.04	1177.87	9.85	1172.83
BM			1.66	1176.21 (1177.68)

Spk SW root 24' Elm 30' Rt 18+02

81.2	81.5	85.0	1185.3	84.8	81.5	81.3
17.6	12.3	8.8	8.5	9.0	12.3	12.5
30	20.5	12.5		13.5	19	30

1176.8	1179.6	1177.9
5.9	3.1	FL
FL		4.8

Send 3'x3' stone 24+80 35' Rt

	+	A	-	E
T.P.	1.05	1174.28		1172.83
Y6			8.8	1165.5
			11.01	1163.27
T.P.	0.38	1173.21		1172.83
B.M.	1.39	1162.55	12.05	1161.16

culvt

28			5.5	1157
30			11.7	1150.8
T.P.			12.56	1149.99
B.M.	6.85	1168.01		1161.16

sta 28 to 29 wet rdwy

T.P.	0.0	1149.99		1149.99
32			9.0	1141.0
T.P.	0.66	1138.08	12.57	1137.51
33			2.4	1135.7
34			6.6	1131.5
35			8.9	1129.2
36			10.3	1127.8

culvt

T.P.	1.85	1128.18	11.75	1126.33
------	------	---------	-------	---------

Send 2 3x3 stone 24'+80' 235' E1

Horiz. spike SW side 15" Ap. 40' E of #44
don S - Hosford Rd

1153.7	1155.2	1155.6	1158.9	1156.7
8.9	7.4	7.0	3.7	5.9
90	55			FL

1158.1	61.6	63.7	61.0	52.3	50.0	50.2	11.0
	6.4	4.3	7.0	15.7	19.0	17.8	5.0
9.9	100	150	200	300	400	Hosf	FL
				350			

all limbs
of fall

1123.1	1127.2	1124.2
15.0	10.9	13.9
FL		FL

SW 4 W 6 d w l

	+	H I 1128.18	-	E	
38+0			2.2	1126.0	
39+0			8.0	1120.2	
TP	0.31	1118.43	10.06	1118.12	
40+0			7.5	1110.9	
TP	.90	1107.26	12.07	1106.36	
41+0			6.7	1100.6	
TP	- 1.58	1093.28	12.40	1094.86	
42+0			0.70	1092.6	
43+50			9.9	1088.4	Bridge
B.M. MADE			6.50	1086.78	
44+0			6.1	1087.2	
B.M. SET			3.94	1089.34	
46+0			4.5	1088.8	
TP	9.86	1101.08	3.06	1091.22	
48+0			1.5	1099.6	
TP	11.04	1111.04	1.68	1100.00	
TP	12.98	1121.98	2.04	1109.00	
50+0			6.0	1116.00	

1082.7	1082.4	1088.4	1082.5
10.6	FL, 10.9	6	FL 10.8
100'		4.9	

CROSS CUT N.E. TOP SOUTH ^{ABUTMENT} FOUND, BRIDGE ± 43+46

VERT SPR SW. ROOF 20" MAPLE ± 45+92 East Side Road

	20.6	18.6	13.8	115.1	15.4	15.4	13.8	19.9	22.5	
DOWN	1.4	3.4	8.2	6.9	6.6	6.6	8.2	2.1	-0.5	dip out
OUT	28	22	16	13	11	13	17	30	40	

	+	H I	-	ELV
		1121.98		
TP	10.09	1129.71	2.36	1119.62
51+00			6.2	1123.5
52+00			2.1	1127.6
+75			1.5	1128.2
54+00			2.8	1126.9
TP	0.87	1130.4	0.54	1129.17
56+00			7.4	1122.6
58+00			9.8	1120.2
TP	1.66	1121.24	10.46	1119.58
60+00			3.9	1117.3
62+00			9.2	1112.0
TP	0.70	1108.88	13.06	1108.18
3M SET			2.89	1105.99
64+00			3.5	1105.4
+67±				
66+00			5.8	1103.1
68+00			4.2	1104.7
TP	2.97	1108.09	3.76	1105.12
70+00			2.2	1105.9
72+00			3.7	1104.4
74+00			5.4	1102.7
+76±				
76+00			5.5	1102.6
TP	3.00	1105.87	5.22	1102.87
78+00			3.1	1102.8

44

E

VERT Spn W. Road 24" Elm East Side Road ± 63+77

1099.9	1100.4	1104.3	1101.4
← 9.0	F.L. 8.5	4.6	F.L. 7.5
100			

Clean OUTLET

1098.7	1099.5	1102.5	1099.4
9.4	F.L. 8.6	5.6	F.L. 8.7
100			

	+	H1 ✓	-	ELL	
		1105.87			
80+00			7.0	1098.9	
I.P.	4.87	1101.68 ✓	9.06	1096.81 ✓	
B.M. SET			3.49	1098.20 ✓	± 81+23
81+30	CULVERT ± 56' SOUTH CLARK RD ±				

March 28th 1951 TURSIC - LEWIS - MAYNARD - RAIN

BM	0.55	1098.75 ✓		1098.20	± 81+33
83+0			2.5	1096.3 ✓	
84			5.8	1093.0 ✓	
86			8.9	1089.9 ✓	
TP	4.38	1093.42 ✓	9.71	1089.04 ✓	
88+00			4.5	1088.9	

88+95 CULVERT REPAIR (OVER W. END)

B.M. SET			5.09	1088.33 ✓	
90+0			5.0	1088.4	

STOPPED - TOO MUCH RAIN

1:30 PM
3-29-1951 P.M. - TURSIC - MAYNARD

B.M.	3.82	1102.02		1098.20	± 91+23
CLARK ROAD					

BM Fd			3.76	1098.26 (1099.35)	
-------	--	--	------	-------------------	--

□ = Travel &

NW Root	24" MAPLE	EAST Side Road	VERT SPT
1092.1	1094.4	1097.2	1095.0
100' Ken Clark Rd	FL. 7.3	4.5	F.L. 6.7
9.6			

1091.7	1093.0	1091.9
7.1	5.8	6.9
11		19
1088.4	1089.9	1090.0
10.4	8.9	8.8
13.6		18
1087.5	1088.9	1087.2
5.9	4.5	6.2
14		19

1086.7	1088.8	1086.1	85.8	85.1	85.0
FL. 6.7	4.6	OUT FL. 7.3	7.65	838.4	100 100 175

HOR. SPT W Side 8" ELM EAST Side Road ± 89+65

1087.1	1086.9
6.3	6.5
04.5	17

89.5	900	906	922	93.7	1098.26	97.4	99.4	01.4	01.5	00.7
12.5	12.0	11.4	9.8	8.3	3.76	4.6	2.6	0.6	0.5	1.1
500	400	300	200	100	0.4	100	200	300	400	500

Spk 5 root 24" map. 5th east on Clark & N side Clark

	T	H1	-	FLV	
BM	5.48	1093.81		1088.33	± 89+65
92+00			4.7	1089.1	
94+00			5.4	1088.4	
96+00			8.6	1085.2	
TP	0.0	1085.02	8.79	1085.02	
98			4.2	1080.8	
100			7.8	1077.2	
102			10.7	1074.3	
T.P.	0.53	1074.70	10.85	1074.17	
104			6.8	1067.9	
105			8.6	1066.1	
+70		Culvt			
106			9.9	1064.8	
BM	4.38	1069.28	9.80	1064.90	

107+64			2.3	1067.0	
108			3.0	1066.3	

W E 46

1087.8
G.D. 1087.9
5.9

8.0
8.2
5.7
8.6

1060.4 65.3 61.1 60.7
FL 9.4 FL 14.0
14.3 13.6 ± 100 ± 200

Spk E root 7' elm 30' Lt 106+12

107+80 Fr. drain reqd
run SW or SE

1057.7
11.6
Ech
Wch
60.5 ± 300
8.8 10.7

1055.5
13.8
± 450 = confl. Ech & creek

1054.9
± 14.0
± 450 = confl. Wch & creek

1058.6

1069.28

109			8.8	1060.5
110			12.4	1056.9
+37 culvt				
111			13.3	1056.0
112			12.2	1057.1
T.P.	10.56	1068.12	11.72	1057.56
114			6.5	1061.6
116			4.4	1063.7
117			3.3	1064.8
118			3.6	1064.5
120			5.8	62.3
T.P.	2.88	1065.27	5.73	1052.39
122			4.2	61.1
124			4.6	1060.7
126			6.0	1059.3
128			9.0	1056.3
BM			7.78	1057.99
T.P.	0.90	1056.24	9.93	1055.34
130			2.0	1054.2
132+00			8.2	1048.0
134+0			12.5	1043.7
T.P.	6.87	1050.70	12.41	1043.83

W.

E

A7

	1050.7	54.7	56.8	56.3	56.9	54.8	51.2
Good	18.6	14.6	12.5	13.0	12.4	14.5	18.1
Fall.	FL	topop	hdwl		hdwl	topopg	FL

Ref spk SE side 10' elm 45' Lt 127±0

1051.7
4.51052.6
3.6

135416.1

10.1

1040.6

COLBURN

BM

7.22

1043.48

T.P.

1.77

1045.60

1043.83

Culst on colburn

From Co. line Non E

1050.70

H1

ELV

10	42.8	43.6	43.48	45.1	47.5	49.5	50.8
	7.9	7.1	7.22	5.6	3.2	1.2	-0.1
	50	100	B.M.	200	300	400	450

Spt NW side 15" twin Ash 83' NE of X

1037.9

39.9

7.7

5.7

N FL

S FL

1038.0

35.9

33.9

32.2

30.9

7.6

9.7

11.7

13.4

12.7

100

200

300

400

500

1951 PAV'T DEPTHS #4STU

○ = ditch

1+0

2±70

7+65 drive pipe reqd on W (McGuff)

8+0

24±60 drive pipe reqd on E (Kulp)

28

41

46

56

59±50

W

E

49

	0'	2 1/2"	3"	2" 0'	
(12)	10'	7'		5' 7'	(13)

c. Diedrich — drive pipe reqd 12"

	5" sand	2"	1/2"	(10)
(12)	9'		6'	

berm	2" sand	6"	mud	3" sand	(15)
10'	8'		2'	9'	

(15)	6	1/2"	2 1/2"	1" berm	(17)
	13'	8'		10' 14'	

(15)	6	1"	7" gravel	1"	5	(15)
	12'	7'	8" sand	7'	11'	

(16)	2"	5"	1 1/2" 0'	no b	(13)
	9'		5' 8'		

drive pipe reqd
W

68

80

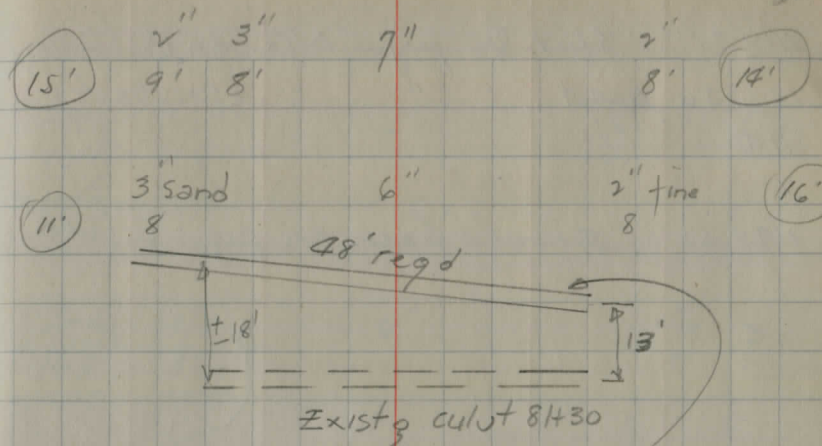
dark Rd

92

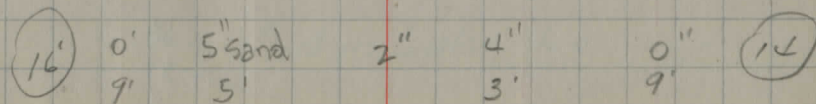
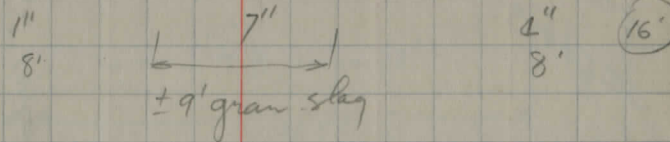
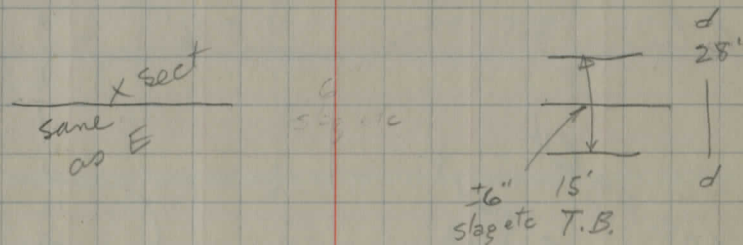
95±80 dr. pipe reqd W (Copperman)

104.

50



better location



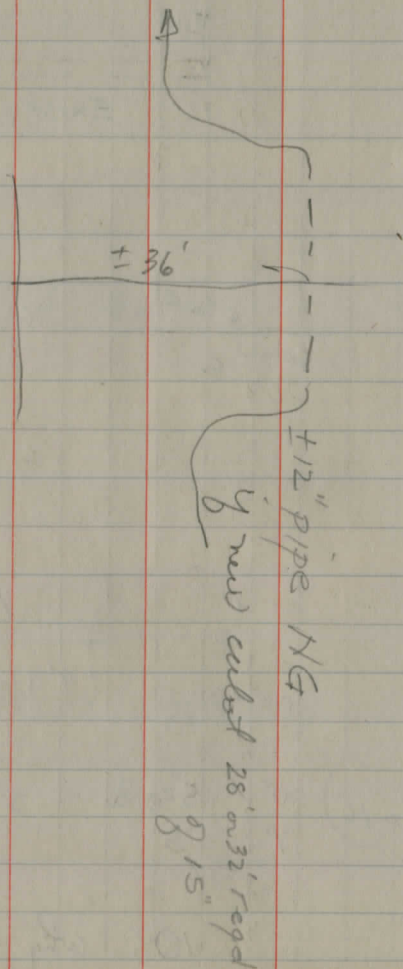
108 why not knock off hump

111 ± 70 East Dr. pipe NG. on E (Lilley)
 113 ± 50 West " " " (Wickert)
 114

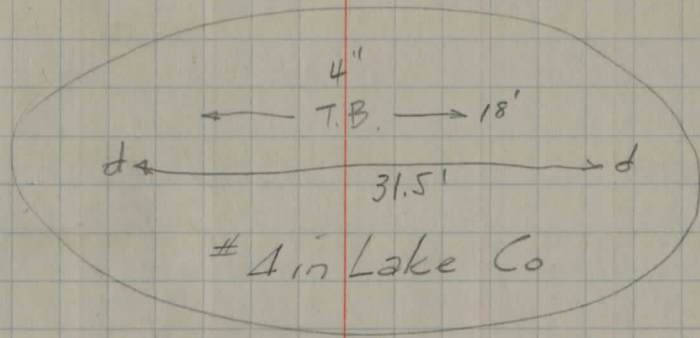
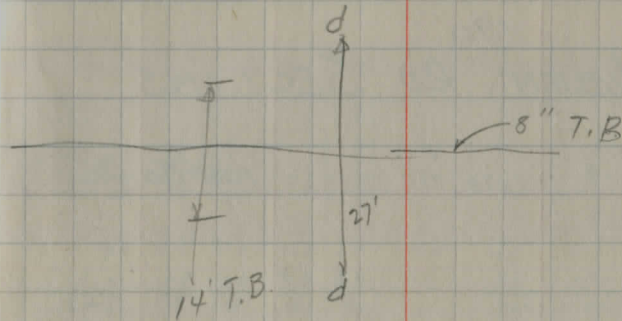
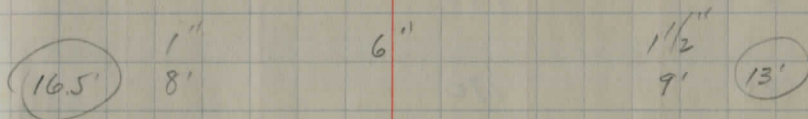
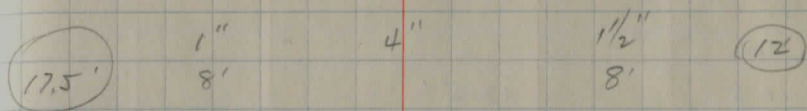
119 ± 55 should have Dr pipe E (Collins)

126

Coline



See pg 64
 for other part
 depths Jan 53



Hill st
sta

108 125'

52 190'

38 170'

11 190'

AUBURN RD SECTIONS

5-15-51

BNT 9.18 1074.08 ✓ 1064.90

103+0

104+0

+04

Triple Elm
17'

+34

CEI.
28'

+42

124 Elm
155

+52

W Elm
155

+89

2 Pine

105+0

+83

6 Elm
15'

106+0

+44

15 Elm
17

Big Elm 106+12

72.5	71.7	70.2	70.5	70.9	1071.4	70.6	69.9	74.6	75.0
1.6	2.9	3.9	3.6	3.2	2.7	3.5	4.2	-0.5	-0.9
36	30	19	14	12	9	13.5	15.17	24	30

67.1	67.0	66.6	67.0	67.9	67.2	66.6	67.2	69.4	70.4
7.0	7.1	7.5	7.1	6.2	6.9	7.5	6.9	4.7	3.7
34	18	17	16	15	12	13.6	15	20	29

63.6	63.1	65.4	65.6	66.1	65.4	64.0	65.1	66.2	65.0	64.7
10.5	11.0	8.7	9.5	8.0	8.7	10.1	9.0	7.9	9.1	9.4
35	26	15	10		11.2	12.15	16	19.2	23	33

63.6	63.9	63.0	64.5	64.8	64.1	63.1	62.7	62.6
10.5	10.2	10.7	9.6	9.3	10.0	11.0	11.4	11.5
34	19	17	16	14	11	14	16	32

TP, 9.47 1074.08 1071.37 1064.90

106+80 $\frac{10^{\circ} \text{APP}}{26}$

106+90

107+0 DRIVE

+60 $\frac{22^{\circ}}{29'}$

+70

NEED TURNING N FOR 100' 24'

108+0

+26

+42

+57

+71

+96

+98

109+0

+20 $\frac{6^{\circ} \text{PINE}}{26'}$

+41

+65

+74

+79

+95

TP, 3.86 1062.22 13.01 1058.36

110+0

+21

$\frac{18^{\circ} \text{ELM}}{23'}$

$\frac{10^{\circ} \text{ELM}}{21.5'}$

$\frac{6^{\circ} \text{ELM}}{19.5'}$

$\frac{7^{\circ} \text{ELM}}{19'}$

$\frac{11^{\circ} \text{ELM}}{21'}$

$\frac{15^{\circ} \text{ELM}}{21'}$

$\frac{12^{\circ} \text{ELM}}{23'}$

$\frac{\text{RAINY CLUMP}}{22'}$

$\frac{13^{\circ} \text{ELM}}{20'}$

$\frac{14^{\circ} \text{ELM}}{20'}$

$\frac{14^{\circ} \text{ELM}}{18'}$

$\frac{12^{\circ} \text{ELM}}{16'}$

H₂O Problem 11
109+70 x 110+70

Big ELM

67.5	66.6	64.4	65.1	65.3	64.3	64.1	65.0	63.6
$\frac{3.9}{32}$	$\frac{4.8}{20}$	$\frac{7.0}{17}$	$\frac{6.3}{14}$	6.1	$\frac{7.1}{13}$	$\frac{7.3}{14}$	$\frac{6.4}{17}$	$\frac{7.8}{32}$

67.3	65.5	65.5
$\frac{4.1}{40}$	$\frac{5.4}{17}$	$\frac{5.4}{17}$

69.2	68.0	66.3	66.6	66.9	65.9	67.9	66.7	66.8
$\frac{2.2}{33}$	$\frac{3.0}{20}$	$\frac{5.1}{14}$	$\frac{4.8}{12}$	4.5	$\frac{5.5}{13}$	$\frac{3.5}{18}$	$\frac{4.7}{21}$	$\frac{4.6}{37}$

68.6	67.4	66.2	65.6	65.8	66.2	65.2	67.8	67.2	66.7	67.0
$\frac{2.8}{36}$	$\frac{4.0}{20}$	$\frac{5.2}{18}$	$\frac{5.9}{14}$	$\frac{5.6}{18}$	5.2	$\frac{6.2}{14}$	$\frac{3.6}{19}$	$\frac{4.2}{30}$	$\frac{4.7}{32}$	$\frac{4.6}{39}$

63.8	63.4	62.7	60.3	59.6	59.9	60.5	59.4	60.2	62.1	63.0	61.8	61.0
$\frac{7.6}{35}$	$\frac{8.0}{25}$	$\frac{8.7}{21}$	$\frac{11.1}{17.5}$	$\frac{11.9}{15}$	$\frac{11.5}{13}$	10.9	$\frac{12.0}{12}$	$\frac{11.2}{18}$	$\frac{9.3}{19}$	$\frac{5.4}{21}$	$\frac{9.6}{28}$	$\frac{10.4}{38}$

H₂O

55.0	55.5	56.3	56.2	56.8	55.8	55.9	54.5	54.2
$\frac{7.2}{33}$	$\frac{6.7}{21}$	$\frac{5.9}{17}$	$\frac{6.0}{13}$	6.4	$\frac{6.4}{13}$	$\frac{6.3}{15}$	$\frac{7.7}{24}$	$\frac{7.0}{34}$

11140

+ 65

DRIVE

11240

B.M. 43+46

12.24

1099.02

1086.78

44+0

43+0

42+0

TP.

12.66

1110.61

1.07

1097.95

41+0

TP.

12.22

1122.33

0.10

1110.61

40+0

39+0

TP.

9.37

1130.34

1.86

1120.97

39+0

39+85

END FENCE

480

CEI
29

38+52

38+50

+ 28

END FENCE

CEI
29

1071-5000
30

54.4 55.2 54.7 55.4 56.0 56.3 54.3 55.4 55.8

7.8 7.0 7.5 6.8 6.2 6.9 7.9 6.8 6.0

30 19 17 15 11 13 14 AND 14 15 18 32 31

57.4 58.2 57.6 55.5 56.2 57.0 56.4 56.0 58.6 59.3

4.5 4.0 4.6 6.7 6.0 5.2 5.8 6.2 3.6 2.9

33 22 30 17 16 5 11 12 13 15 30

X N.E. Top South Abutment of Bridge

84.5 86.3 1087.2 86.6 84.5 84.2

14.5 14.5 12.7 11.3 12.0 14.5 14.8

27 17 13 10 17 30

87.1 87.4 88.3 88.4 87.8 88.6 1089. 88.4 88.4 88.0 87.6

11.9 11.6 10.7 10.6 11.2 10.8 10.0 10.6 10.6 11.0 10.4

29 23 21 16 15 14 12 15 17 30

95.1 91.1 91.6 1092.5 91.7 91.1 92.3 92.0

4EV 3.9 7.9 7.4 6.5 7.3 7.3 7.4 6.7 7.0

28 15 14 13 14 15 17 21 31

1102.5 1101.5 1099.1 1100.0 1100.5 1099.8 98.7 1101.1 1101.2

down 42 8.1 8.1 11.5 10.6 10.1 10.8 11.9 9.5 9.4

29 21 15 13 15 16 17 23 30

15.6 08.8 10.1 1110.7 09.6 08.9 12.9 14.3

down 42 Fence 7.2 14.0 12.7 12.1 13.2 14.0 9.9 8.5

30 28 16 15 12 14 15 21 28

19.2 1120.1 19.2 18.4 19.6 18.1

3.6 2.7 3.6 4.6 3.2 4.7

12 13.2 15 16 14

23.5 1123.9

down 42 6.8 6.4

Fence 30 25

25.6

4.7

Fence 30 down 42

23.7 22.5 1123.4 22.4 22.0 21.3

6.6 7.8 6.9 7.9 8.3 6.0

404 28 13 15 14 30 Fence

7 Barn Yard

down 42

38+0

16' MAPLE
29'

37+85

START
FENCE
27'

37+74

37+62

37+54

37+50

37+24

LILAC

27

19 MAPLE

31

LILAC

29

DRIVE

37+0

36+0

TP.

6.77

1134.61

2.50

1127.84

34490 B.A. SET

3.71

1130.90

B.M. 45+92

6.33

1095.67

1089.34

45+0

46+0

N.E. END

FENCE STOP 27'

7.89

700 PINE
20'

47+0

TP.

11.55

1106.57

0.65

1095.02

25.3	24.7	1125.7	24.9	30.1	31.1
5.0	5.6	4.6	5.4	0.2	-0.8
FACE TOOL	SPCS	39	14	26	33

23.8	24.6	24.3	24.5	25.8	25.6	1126.7	26.4	26.0	26.6	29.5
6.5	5.7	6.0	5.8	4.5	4.7	3.6	3.9	4.3	3.7	0.8
30	25	23	18	14	13		14	15	19	37

24.1	24.2	25.9	1127.0	26.5	25.3	26.4	28.1
FENCE	6.2	6.1	4.0	3.8	5.0	3.9	2.2
27	29	19	14	14	18	20	34

23.5	26.7	1127.6	27.0	26.0	26.9	28.1	29.5	
DOWN STAKE	6.8	3.6	2.7	2.3	4.3	3.0	2.2	0.8
FENCE	26	12		15	17/18	20	24	32

VERT Spt NW Root 28" SHAG 20' EAST

VERT Spt S.W. ROOT 20" MAPLE E. SIDE OF ROAD

85.3	85.6	85.6	86.3	1087.2	86.5	86.0	85.7
10.4	10.2	10.1	9.4	8.5	9.2	9.7	10.0
DOWN 2 FENCE	26	18	15	12	11	14	31

87.0	87.8	1088.9	88.0	87.2	87.8	88.2	87.7	88.7	89.2
8.7	7.9	6.8	7.7	8.5	7.9	7.5	8.0	7.0	6.5
30	15		11	15/16	17	19	23	26	52

92.6	93.4	91.5	92.1	1092.8	92.2	90.9	92.5	94.9
9.1	2.3	4.2	3.6	2.9	3.5	4.8	3.2	0.8
30	30	16	14		12	15/16	20	27

LEV

AUBURN ROAD GRADES

40+0				
T.P.	6.00	1123.92	12.91	1117.92
+50				
39+0				
T.P.	8.70	1130.88	9.00	1122.63
+50				
38+0				
+50				
37+0				
36+50				
BM	0.73	1131.63		1130.90

WEST



EAST

56

17.6	15.5	13.5	1110.7	27.5	15.1	14.3	16.3
6.3	8.4	10.4	13.2	9.8	9.6	7.6	7.6
S	30'	22.5		28'	30'	S	
21.8	19.6	15.7		20.4	22.4		
9.0	11.2	8.2		10.4	8.4		
S	30'			30'	S		
25.3	23.5	23.6	1120.2	23.3	25.5	27.2	
5.5	7.3	7.2	10.6	7.5	5.3	3.6	
S	30'	28'		24'	30'	S	
26.3	23.7	23.6	1123.4	29.4	31.1		
5.3	7.9	8.0	8.2	1.4	+0.3		
S	30'	26'		30'	S		
26.9	24.6	24.7	25.7	30.7	32.8		
4.7	7.0	6.9	5.9	0.95	+1.13		
S	30'	20'		30'	S		
26.7	23.8	24.5	26.7	28.0	29.9	30.6	
4.9	7.8	7.1	4.9	3.6	2.8	1.0	
S	30'	18'		25'	30'	S	
26.7	23.5	25.6	26.9	24.8	27.6	29.7	
4.9	8.1	6.0	4.7	6.8	4.0	1.9	
STK	30'	14'		18'	30'	STK	
26.5	23.4		1127.2		28.1	30.3	
5.1	8.2		4.4		3.5	1.30	
S	30'				30'	S	

+50
T.P. 5.32 1133.42 3.59 1178.10

52

+50

5/40

+50

12.79 1131.69 0.40 1118.90

50+0

T.P. 12.51 1119.30 0.30 1106.79

T.P. 12.71 1107.09 1.21 1096.38

BM 6.25 1095.59 1089.34 ± 45+92

40+50

T.P. 4.38 1115.33 12.97 1110.95

1173.92

W E

E

57

32.2 28.7 1128.1 29.3 32.4
1.2 4.7 5.3 4.1 1.0
5 30 30 5

31.0 29.1 29.3 27.5 29.4 29.6 32.9
-0.7 2.6 2.4 4.2 2.3 2.1 +1.2
5 30 28 24 30 5

32.2 29.1 26.0 29.8 32.1
+0.5 2.6 5.7 1.9 +0.4
5 30 30 5

30.5 28.2 27.9 23.4 26.1 28.3 30.6
1.2 3.5 3.8 8.3 5.6 3.4 1.1
5 30 27 24 30 5

27.6 25.2 1120.0 24.3 26.6
4.1 6.5 11.7 7.4 5.1
5 30 30 5

23.3 20.1 19.9 22.0
8.4 11.6 3.4 15.9 11.8 9.7
5 30 13 41:19.30 16.5 30 5

11.5 09.3 1105.5 06.7 09.0
3.8 6.0 9.8 8.6 6.3
5 30 30 5

104

1070.34

+50

103

78.56

1072.12

6.44

107+50

9.69

1078.56

2.76

1068.87

BM

6.73

1071.63

1064.90

106+12

+50

54

+50

53

1133.42

$$\begin{array}{r} \downarrow \\ 69.8 \\ 8.8 \\ \hline 5 \end{array}$$

$$\begin{array}{r} W \\ 66.9 \\ 11.7 \\ \hline 30 \end{array}$$

$$\begin{array}{r} E \\ 1068.0 \\ 10.6 \end{array}$$

E

$$\begin{array}{r} 70.6 \\ 8.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 58 \checkmark \\ 72.5 \\ 6.1 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 72.7 \\ 72.9 \\ 5.9 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 71.0 \\ 7.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 69.6 \\ 9.0 \end{array}$$

$$\begin{array}{r} 72.9 \\ 5.7 \\ \hline 30 \end{array}$$

$$\begin{array}{r} \checkmark \\ 76.1 \\ 2.5 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 75.1 \\ 75.9 \\ 2.9 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 72.5 \\ 6.1 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 71.4 \\ 7.2 \end{array}$$

$$\begin{array}{r} 74.7 \\ 3.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} \checkmark \\ 76.9 \\ 1.7 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 75.3 \\ 3.3 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 72.9 \\ 5.7 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 1073.1 \\ 5.5 \end{array}$$

$$\begin{array}{r} 75.3 \\ 3.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 77.9 \\ 0.7 \\ \hline 5 \end{array}$$

Big Elm

$$\begin{array}{r} 29.9 \\ 3.5 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 26.7 \\ 6.7 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 1125.8 \\ 7.6 \end{array}$$

$$\begin{array}{r} 26.0 \\ 7.4 \end{array}$$

$$\begin{array}{r} 29.4 \\ 4.0 \end{array}$$

$$\begin{array}{r} 30.8 \\ 7.6 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 27.4 \\ 6.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 27.3 \\ 6.1 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 26.8 \\ 6.6 \end{array}$$

$$\begin{array}{r} 26.8 \\ 6.6 \\ \hline 20.5 \end{array}$$

$$\begin{array}{r} 26.5 \\ 6.9 \end{array}$$

$$\begin{array}{r} 30.0 \\ 3.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 31.0 \\ 2.4 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 27.9 \\ 5.5 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 27.5 \\ 5.9 \end{array}$$

$$\begin{array}{r} 27.5 \\ 5.9 \end{array}$$

$$\begin{array}{r} 30.9 \\ 2.5 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 31.5 \\ 1.9 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 28.3 \\ 5.1 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 28.4 \\ 5.0 \\ \hline 22.5 \end{array}$$

$$\begin{array}{r} 1128.0 \\ 5.4 \end{array}$$

$$\begin{array}{r} 27.7 \\ 5.7 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 28.4 \\ 5.0 \end{array}$$

$$\begin{array}{r} 30.7 \\ 2.7 \\ \hline 30 \end{array}$$

W E E

+50

TP, 6.47 1070.73 6.15 1064.26

108+0

+50

107+0

+50

106+0

66.78

+50

105+0

68.56

BM.

5.51

1070.41

1064.90

106+12

104+50

1078.56

W E

67.1 66.8
 $\frac{3.6}{5}$ $\frac{3.9}{30}$

69.7 68.2
 $\frac{0.7}{5}$ $\frac{2.2}{30}$

69.0 68.6
 $\frac{1.4}{5}$ $\frac{1.8}{30}$

67.9 65.5
 $\frac{2.5}{5}$ $\frac{1.9}{30}$

65.2 63.5
 $\frac{5.2}{5}$ $\frac{6.9}{30}$

66.3 63.4
 $\frac{4.1}{5}$ $\frac{7.0}{30}$

66.2 63.6
 $\frac{4.2}{5}$ $\frac{6.8}{30}$

66.3 64.4
 $\frac{12.3}{5}$ $\frac{14.2}{30}$

1063.5
 72

66.1
 43

66.6
 38

65.5
 49

64.8
 56

64.8
 56

65.5
 49

66.1
 43

1066.8
 11.8

64.8 65.5
 $\frac{5.9}{30}$ $\frac{5.2}{5}$

67.2 67.9
 $\frac{3.2}{30}$ $\frac{2.5}{5}$

66.1 67.4
 $\frac{4.3}{30}$ $\frac{3.0}{5}$

64.4 66.1
 $\frac{6.0}{30}$ $\frac{4.3}{5}$

62.3 64.0
 $\frac{8.1}{30}$ $\frac{6.4}{5}$

62.7 65.8
 $\frac{7.7}{30}$ $\frac{4.0}{5}$

63.7 65.4
 $\frac{6.7}{30}$ $\frac{5.0}{5}$

64.8 68.0
 $\frac{5.6}{30}$ $\frac{2.4}{5}$

67.2 70.4
 $\frac{11.4}{30}$ $\frac{8.2}{5}$

7-21-51

Culvt 74+76 After new

8.05

Exist culvt 64+67 north to
new 15" culvt =

+50

109+0

1070.73

18" conc pipe placed

outlet FL	Ground	Stks
50' W	7.96	3.91
100' "	8.51	4.68
50' W	8.87	5.17
200' W	9.10	5.48
250' "	9.36	

59.5

$$\begin{array}{r} 11.2 \\ 5 \\ \hline \end{array}$$

59.2

$$\begin{array}{r} 11.5 \\ 30 \\ \hline \end{array}$$

1058.1

12.4

58.8

$$\begin{array}{r} 11.9 \\ 30 \\ \hline \end{array}$$

59.4

$$\begin{array}{r} 11.3 \\ 5 \\ \hline \end{array}$$

63.6

$$\begin{array}{r} 7.1 \\ 5 \\ \hline \end{array}$$

63.2

$$\begin{array}{r} 7.5 \\ 30 \\ \hline \end{array}$$

1060.4

10.3

61.3

$$\begin{array}{r} 9.4 \\ 30 \\ \hline \end{array}$$

62.0

$$\begin{array}{r} 8.7 \\ 5 \\ \hline \end{array}$$

Sta.	+ BS	HI	- FS	Elev
BM ₁	6.63	95.97		1089.34
46+00			3.9	92.07
45+50			5.4	90.57
45+00			6.6	89.37
44+50			7.2	88.77
44+00			7.9	88.97
43+50			7.5	88.47
43+00			6.6	89.37
42+50			4.6	91.37
42+00			2.2	93.77
T.P.	9.81	100.88	4.90	91.07
41+50			4.0	96.88
41+00			0.3	100.58
T.P.	10.20	110.66	0.42	100.46
40+50		12.23	5.0	105.66
40+00			0.4	110.26
T.P.	0.46	98.89	12.23	98.43
T.P.	2.06	93.77	7.18	91.71
B.M. ₁			4.42	1089.35
BM ₁	8.54	97.88		1089.34
46+50			4.1	93.78
47+00			2.0	95.88
T.P.	10.31	07.75	0.44	97.44
47+50			9.5	98.26
48+00			6.9	100.85

Levels on fill - Sec. STU-CH. #4

Temple 1
Bender X
8-21-51

61

BM Vert. Spk SW root 20" Maple 45+92 E. side of road

	B.S.	HI	FS	Elev.
48+50		0775	3.8	103.95
49+00			0.1	107.65
T.P.	9.29	16.61	0.43	107.32
49+50			4.8	111.81
50+00			1.1	115.51
T.P.	0.84	05.63	11.82	04.79
T.P.	1.03	96.42	10.24	95.39
BM ₁			7.07	1089.35

BM ₂	533	70.23		1064.90
T.P.	7.44	74.42	3.25	66.98
102+00			0.1	74.32
102+50			1.3	73.12
103+00			2.7	71.72
103+50			4.1	70.32
104+00			5.2	69.22
104+50			6.3	68.12
105+00			7.2	67.22
105+50			8.1	66.32
106+00			8.5	65.92
BM ₂	456	69.46	9.52	64.90
106+50			3.9	65.36
107+00			4.3	65.16
107+50			5.1	64.36
108+00			6.3	63.16

108+50		7.7	61.76
109+00		9.5	59.96
109+50		10.8	58.66
110+00		11.7	57.76
110+50		12.5	56.96
111+00		13.1	56.36
111+50		12.9	56.56
112+00		12.5	56.96
BM	69.46 -2.5	4.56	1064.90

1-9-53 Soundings to determine
depth of rock on
NO 4 S
Stafford Hill

1140

3" down
hard sandstone
in ditch \pm 1' deep

1' down
soft sandstone
in ditch \pm 8" deep

10450

1' 10" down
red sandstone
in ditch \pm 8" deep

1.5 down
sandstone
in ditch \pm 8" deep

10

3' down
no rock
edge part

2' - 10" down
no rock
in ditch \pm
10" deep

9450

3' 2" down
no rock
edge part

2.7 down
no rock
ditch \pm 1'
dee

940

3' down
no rock
edge part

2.5 down
no rock
in ditch \pm
1' below crown

8450

3' down
No rock
at edge part

2.5 down
no rock
edge part

W

E

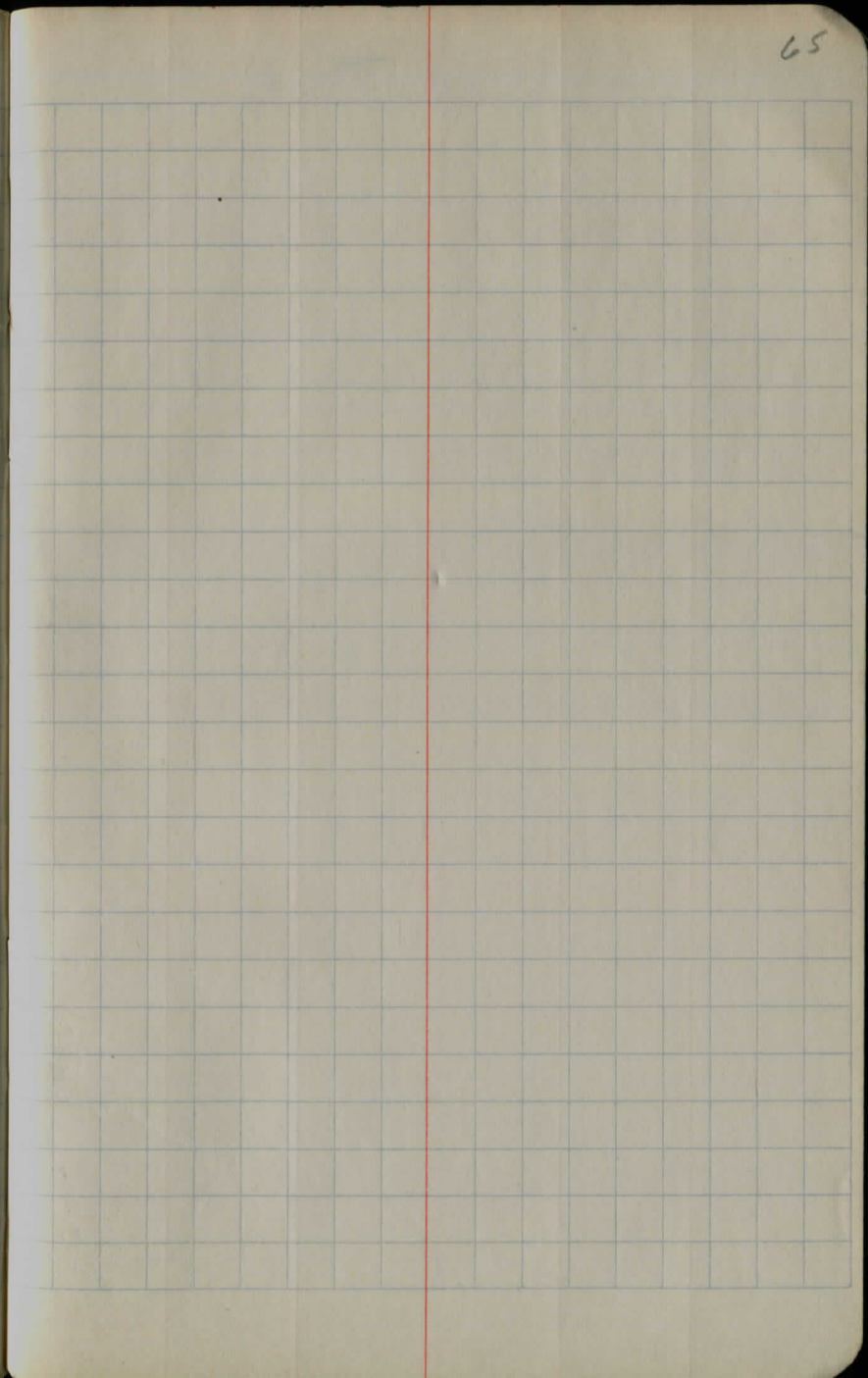
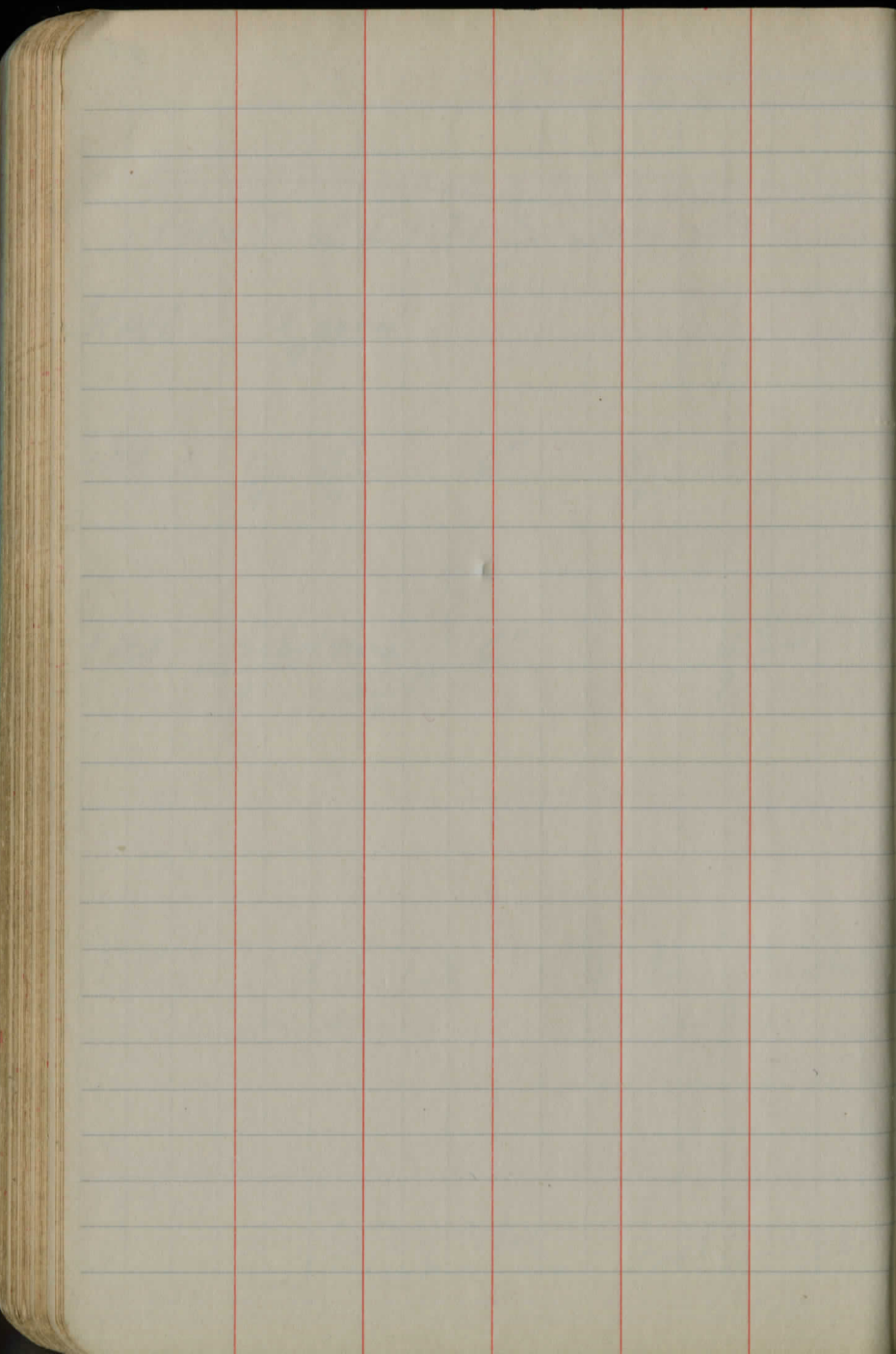
E

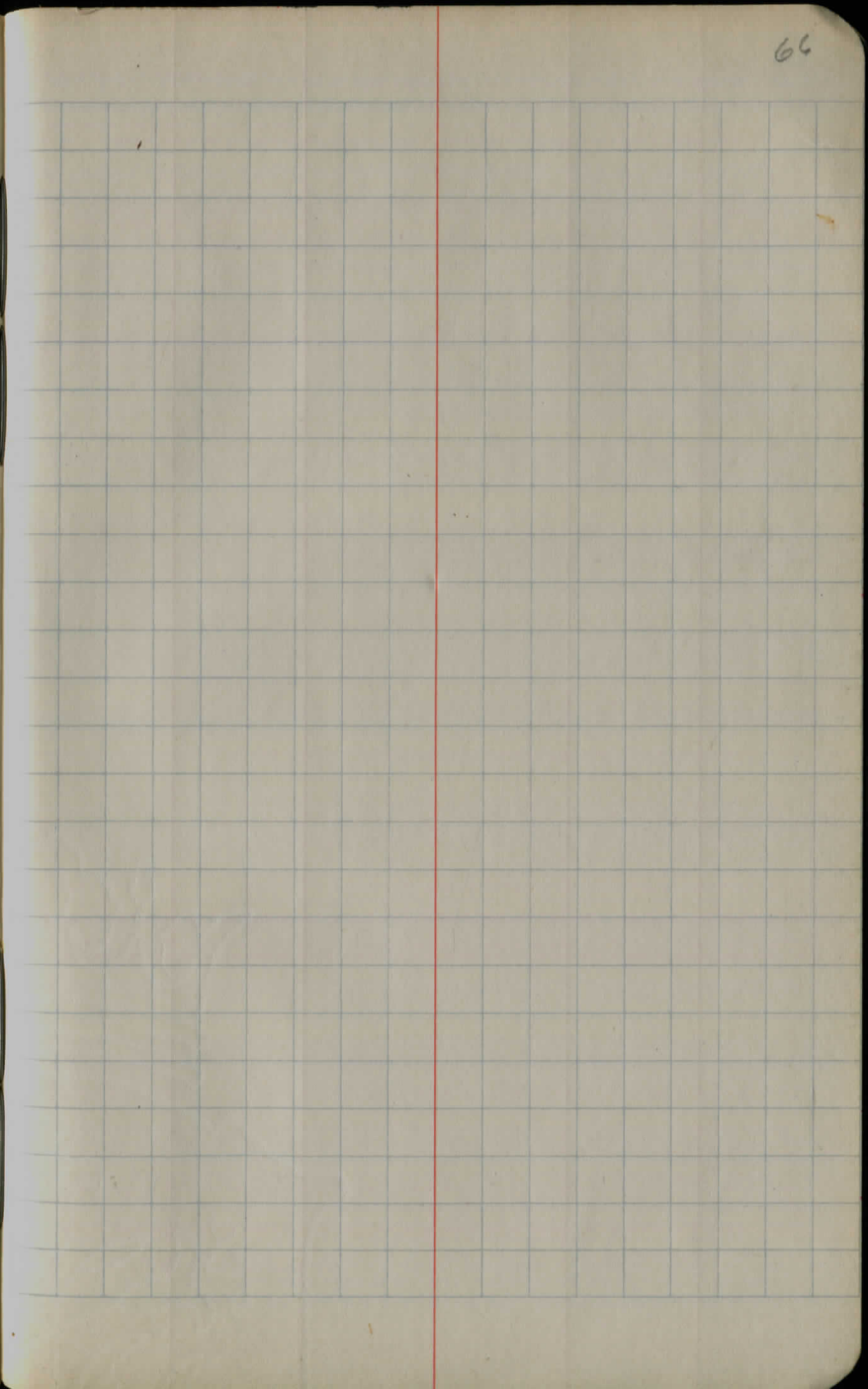
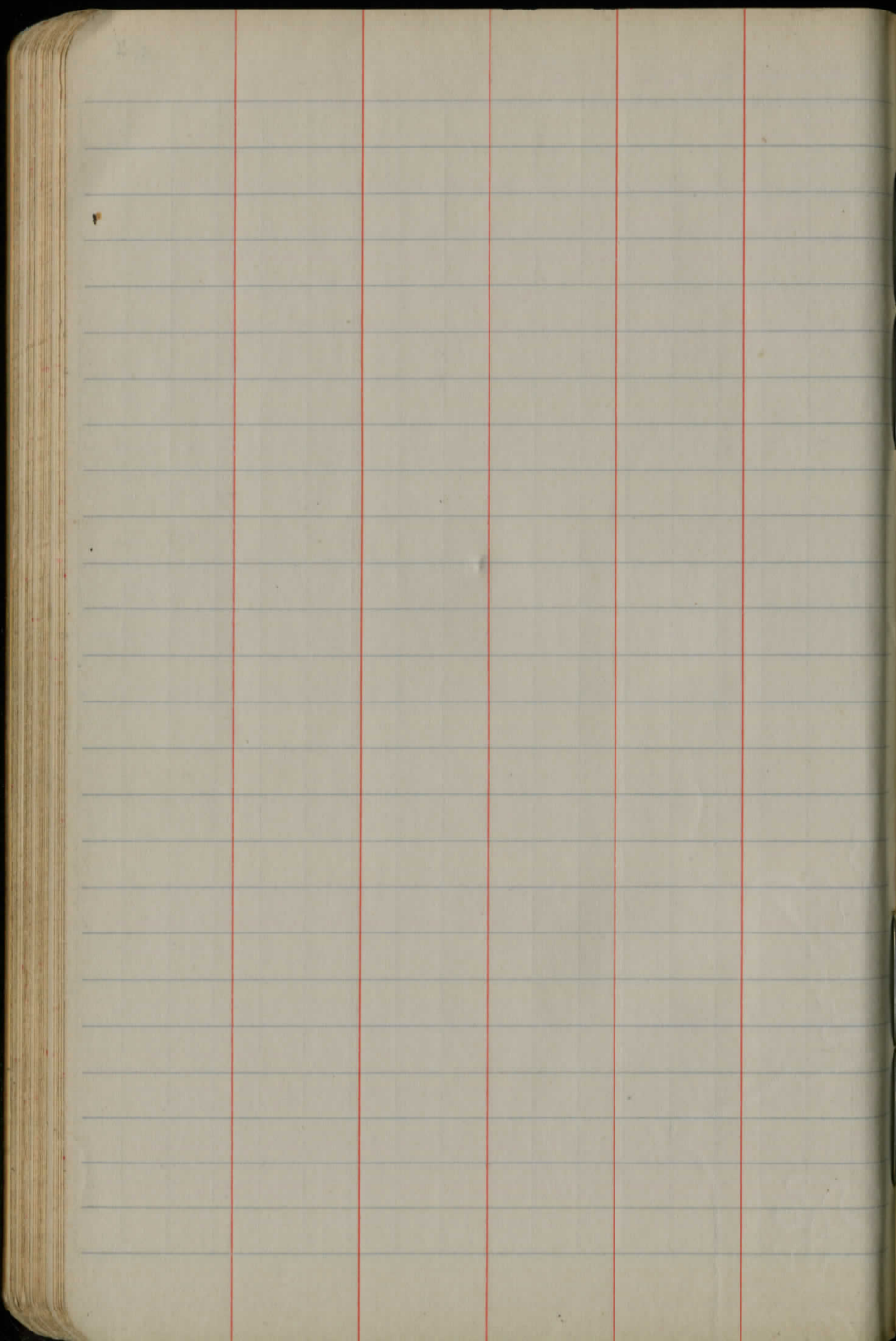
63

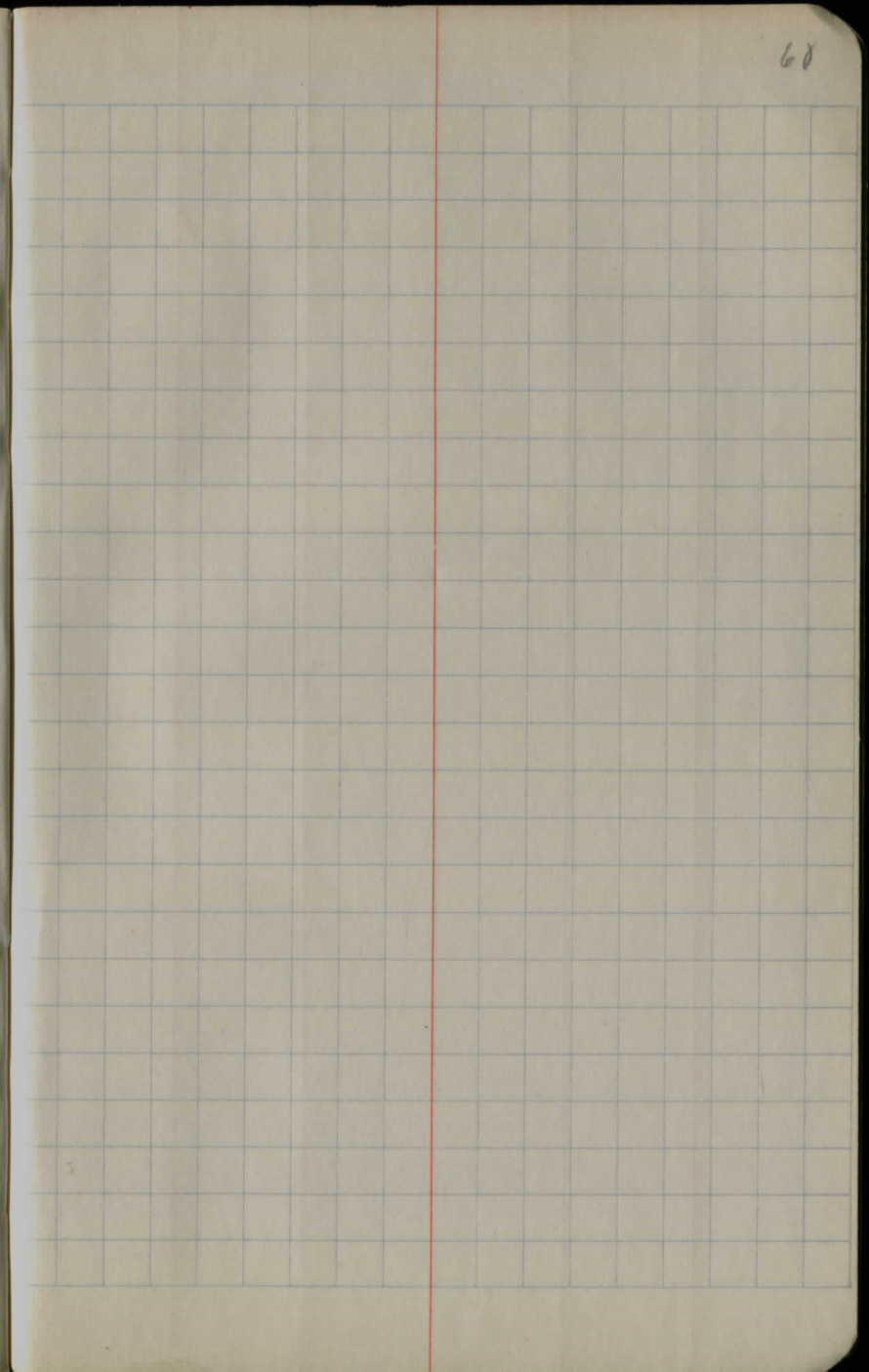
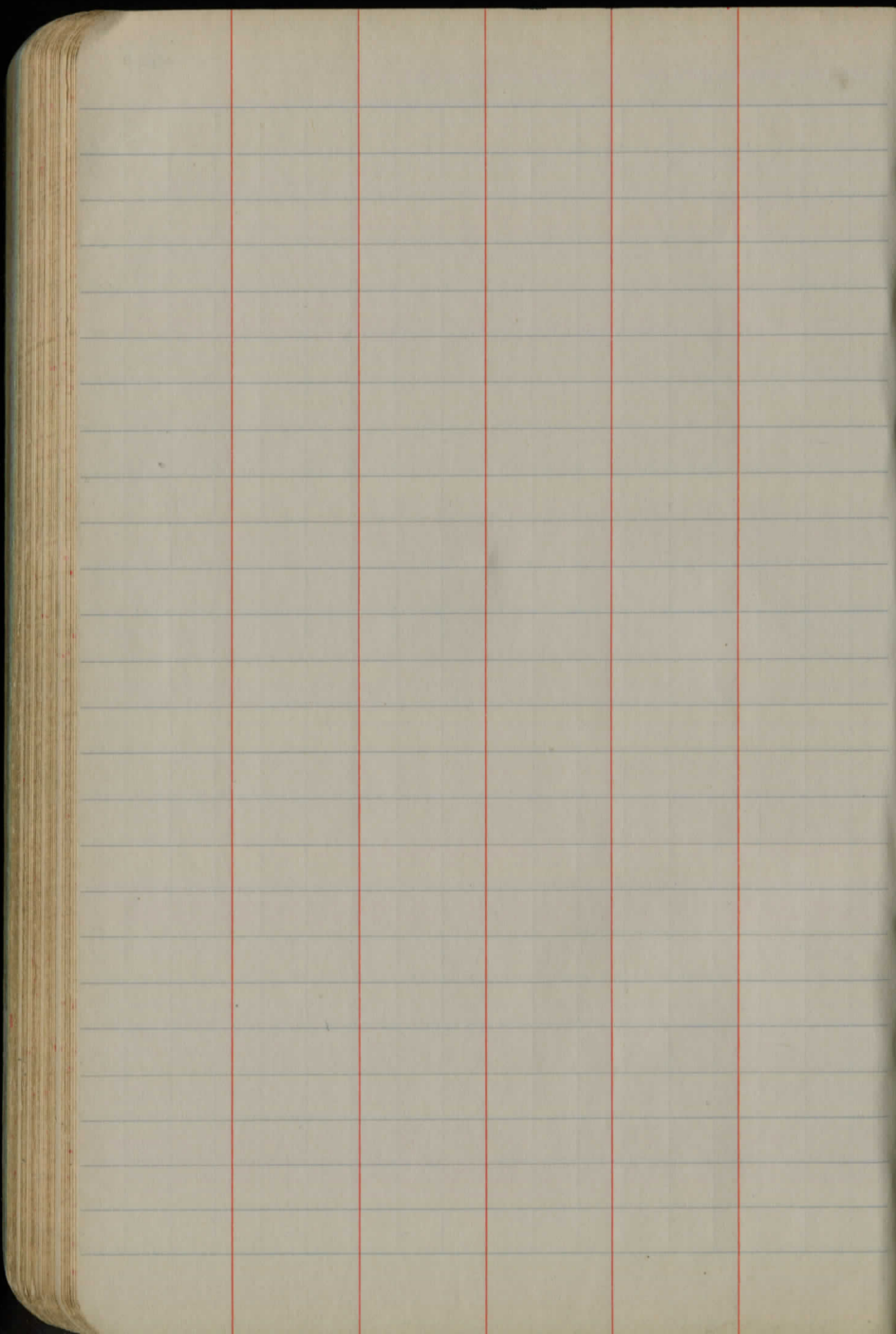
PAV'T DEPTHS Jan 53

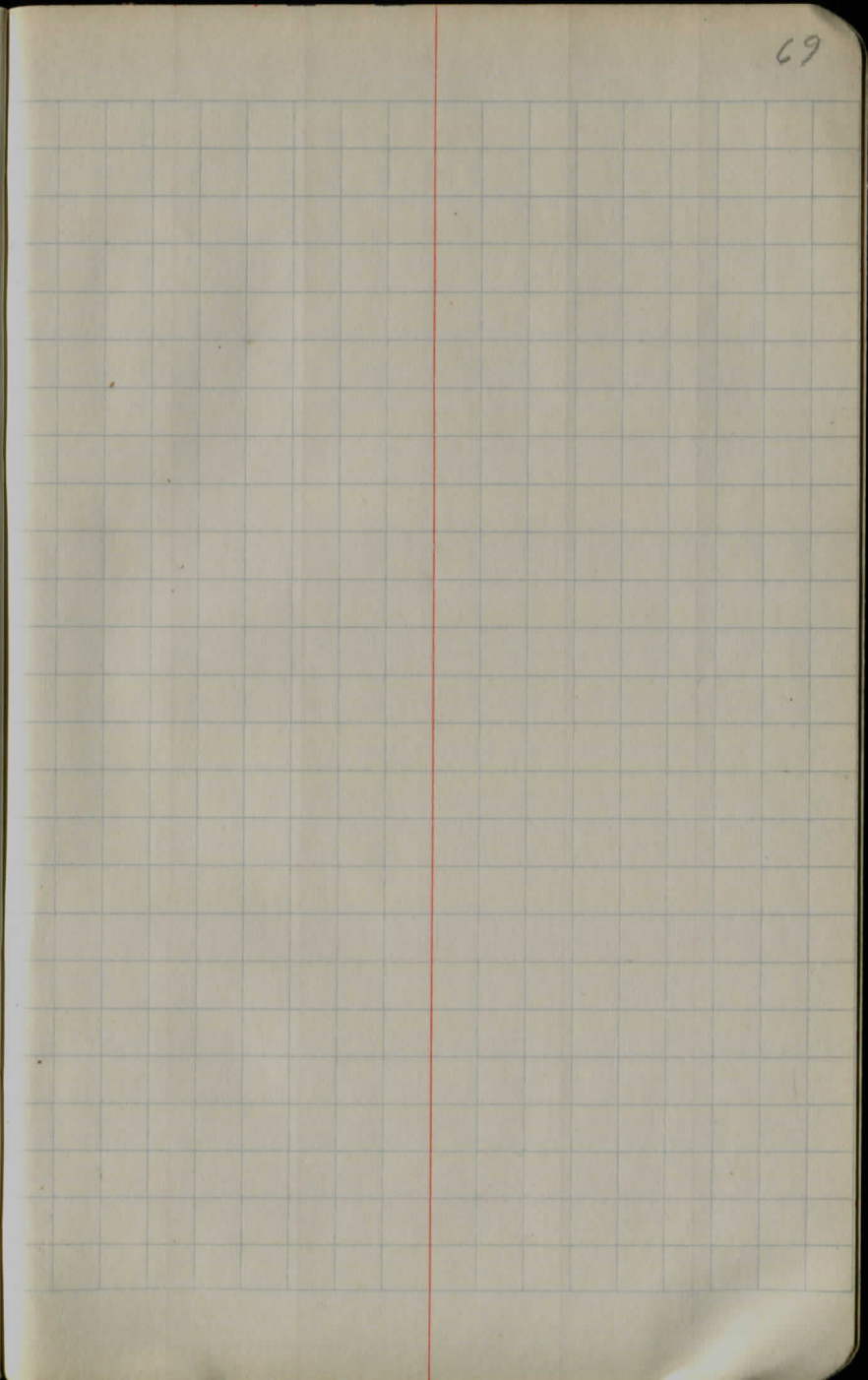
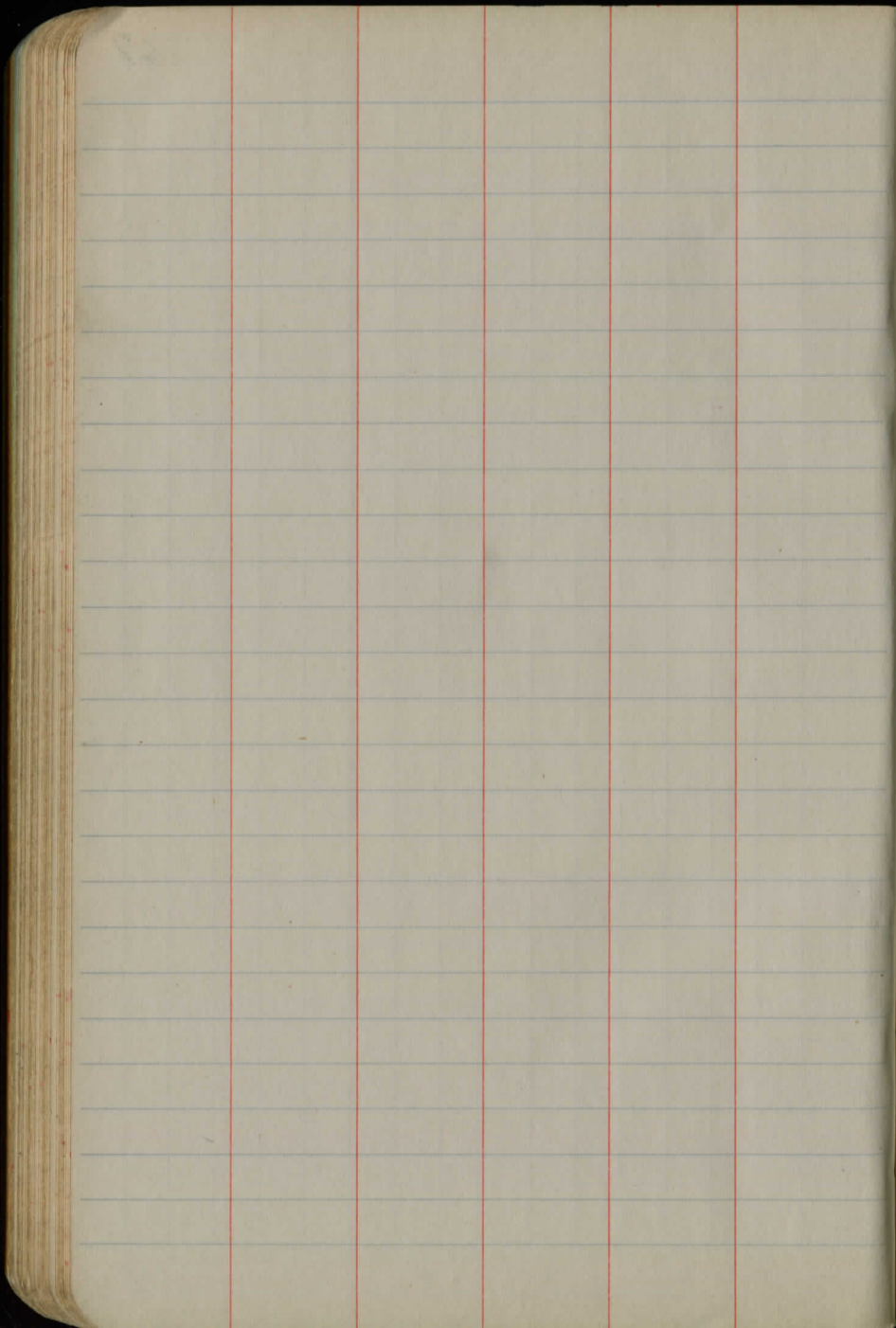
E

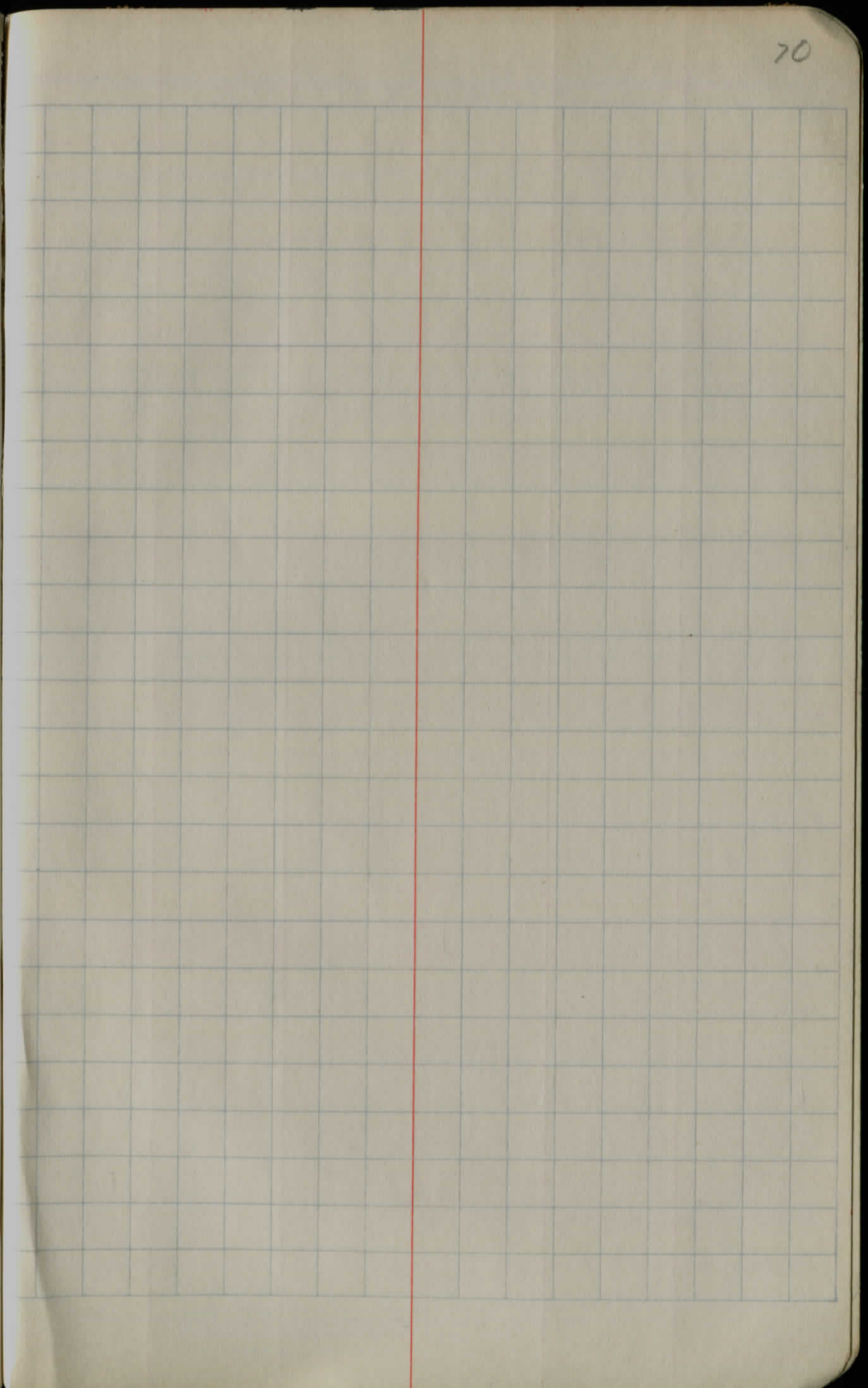
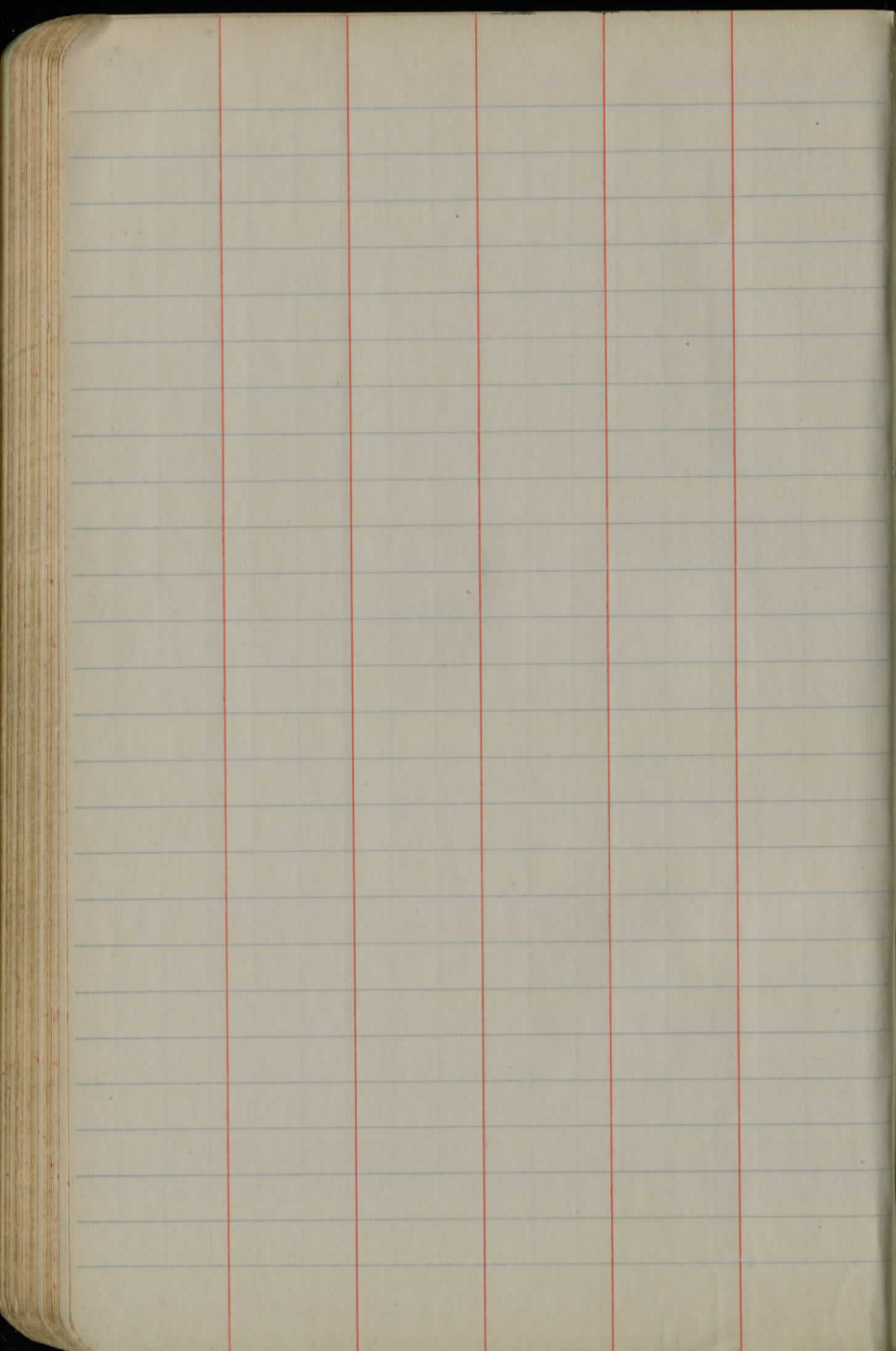
Stall 8" sand
9'±38 0' 3" 6" 3" 1"
9' 7' 7' 9'±108 2" cob & stone 6" 4"
9' 3" cgs 9'12±50 5" down rock 5" down to rock
on berm on berm12±0 3" down 0"
in ditch 15" deep rock in ditch
hard? rock 15" deep

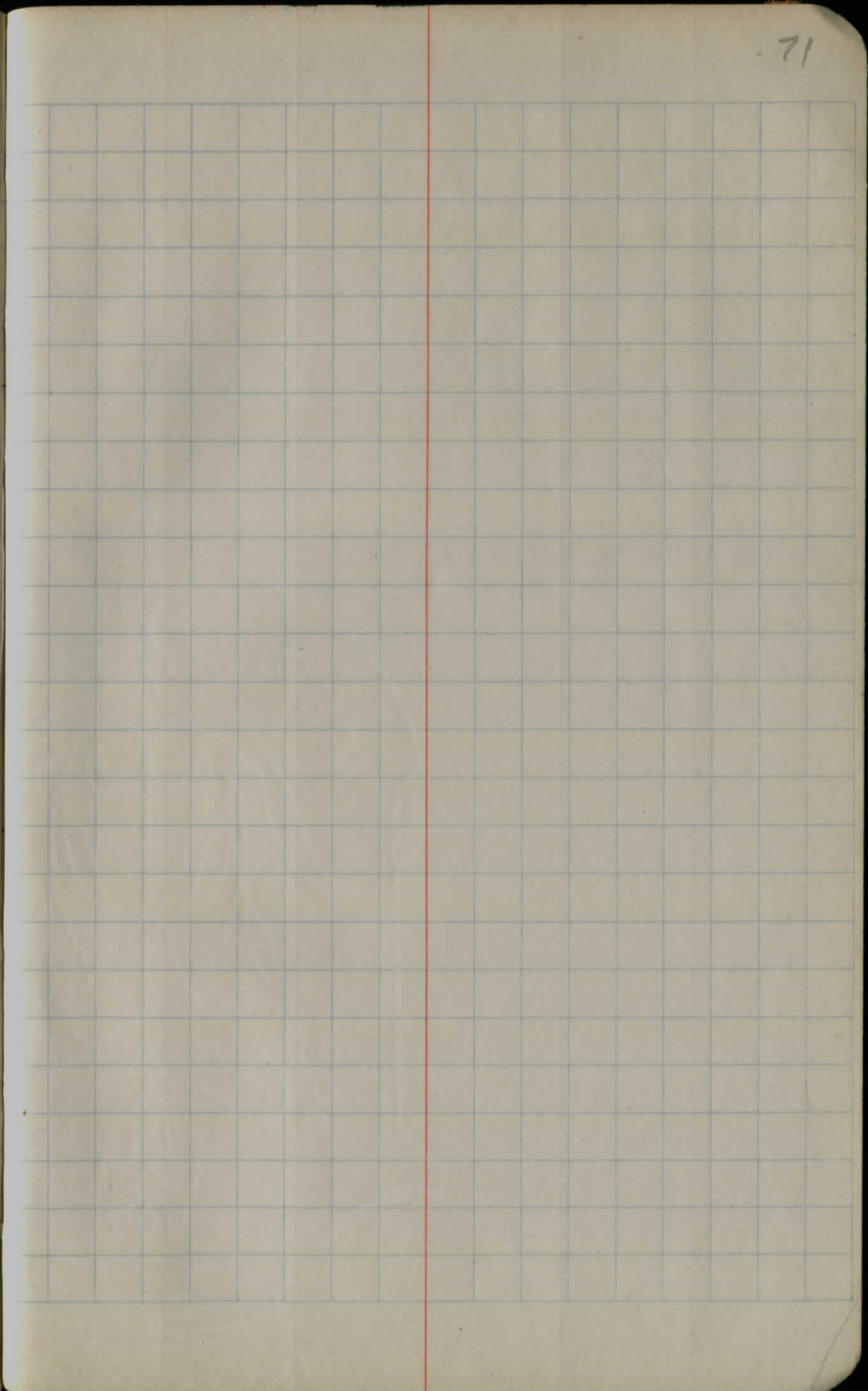
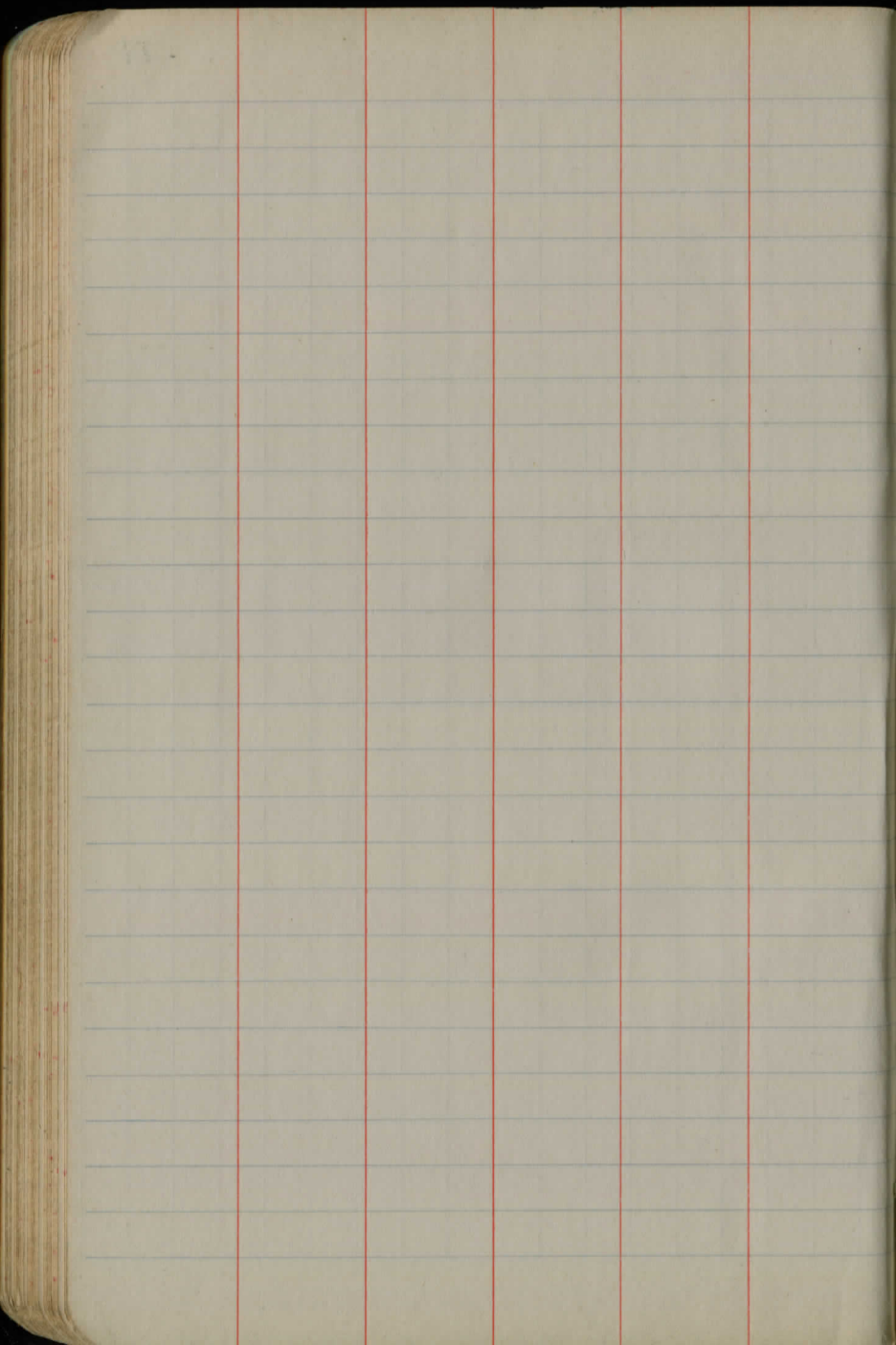












35.97 Δ
collins

Δ 29.82

Δ

30.44 Δ Gittinger
29.90

Δ

31.87 Δ Lilly
30.88

Schweid
Dickle

Δ 26.30

BM S root 24" Elm NW $\frac{1}{4}$ of #4.

See pg 13

BM Spk S root 20" Map 5th tree

" Spk NW root 12" Hick 26' Rt

#No 5 1283.91 = ^{run} From Route #6
up #4 77

on Lt (H?) from X #1 & #77 1099.35

(5) Sta 36+86 on Clark Rd #77 Sec A
= ± 1276' W of #4 1090.12

4.85 = $\frac{1}{2}$ W walls.
 5.05 = L to W 2.65 West of spike
 5.10 = L to E 23.50 to pipe
 5.40 = " " " 30.16 to pipe
 5.45 " " W 27.55 to pipe
 5.75 = Mulb & rd

length .9

KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle
 of Intersection or I. P.= $23^{\circ} 20'$ to the R. at Station
 542+72.

Ext. in Tab. IV opposite $23^{\circ} 20'$ =120.87
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20'$ =1183.1
 $1183.1 \div 10 = 118.31$.

Tab. V. correction for A. $23^{\circ} 20'$ for a 10° Cur.=0.16
 $118.31 + 0.16 = 118.47$ =corrected Tangent.

(If corrected Ext. is required find in same way)
 Ang. $23^{\circ} 20'$ = $23.33^{\circ} \div 10 = 2.3333$ =L. C.

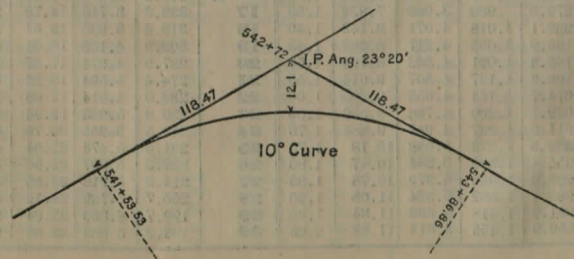
$2^{\circ} 19\frac{1}{2}'$ =def. for sta.	542	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}'$ = " " "	+50	Tan.=	1.18.47
$7^{\circ} 19\frac{1}{2}'$ = " " "	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}'$ = " " "	+50	L. C.=	2.33.33
$11^{\circ} 40'$ = " " "	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3'$ (def. for 1 ft. of 10° Cur.)= $139.41'$ =
 $2^{\circ} 19\frac{1}{2}'$ =def. for sta. 542.

Def. for 50 ft.= $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft.= $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve

(These tables are published in Field Books of
 KEUFFEL & ESSER Co., New York, N. Y.)



11/18/63 Lyle Battles
says stone mon E + of
Brooklane & Ferry Rd
has been knocked out.

Set I.P. within next 6 mo.

See Bk 45 pg 35

Lyle says pear tree is gone

Lyle thinks Jim Post has
other ref.

V 7 Pg 3 #66

V 8 Pg 53

TABLE I. — Minutes in Decimals of a Degree.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	1/8	3-16	1/4	5-16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
0° 10'	34377.	.036	.145	.291	0.05'	7°	819.0	1.528	6.105	12.21	2.10'
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	50	716.8	1.746	6.976	13.95	2.40
1 10	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
20	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
30	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
40	3819.8	.327	1.309	2.618	0.45	50	637.3	1.965	7.846	15.69	2.70
50	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
2 10	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
20	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
30	2644.6	.473	1.891	3.781	0.65	50	573.7	2.183	8.716	17.43	3.00
40	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
50	2292.0	.545	2.181	4.363	0.75	11	521.7	2.402	9.585	19.16	3.30
3 10	2148.8	.582	2.327	4.654	0.80	20	499.1	2.511	10.02	20.04	3.45
20	2022.4	.618	2.472	4.945	0.85	30	478.3	2.620	10.45	20.91	3.60
30	1910.1	.655	2.618	5.235	0.90	40	459.3	2.730	10.89	21.77	3.75
40	1809.6	.691	2.763	5.526	0.95	50	441.7	2.839	11.32	22.64	3.90
50	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
4 10	1637.3	.764	3.054	6.108	1.05	40	410.3	3.058	12.18	24.37	4.20
20	1562.9	.800	3.199	6.398	1.10	50	396.2	3.168	12.62	25.24	4.35
30	1495.0	.836	3.345	6.689	1.15	15	383.1	3.277	13.05	26.11	4.50
40	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
50	1375.4	.909	3.635	7.271	1.25	40	359.3	3.496	13.92	27.84	4.80
5 10	1322.5	.945	3.781	7.561	1.30	50	348.5	3.606	14.35	28.70	4.95
20	1273.6	.982	3.926	7.852	1.35	17	338.3	3.716	14.78	29.56	5.10
30	1228.1	1.018	4.071	8.143	1.40	18	319.6	3.835	15.64	31.29	5.40
40	1185.8	1.055	4.217	8.433	1.45	19	302.9	4.155	16.51	33.01	5.70
50	1146.3	1.091	4.362	8.724	1.50	20	287.9	4.374	17.37	34.73	6.00
6 10	1109.3	1.127	4.507	9.014	1.55	21	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	22	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	23	250.8	5.035	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	24	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	25	231.0	5.476	21.64	43.28	7.50
7 10	955.4	1.309	5.234	10.47	1.80	26	222.3	5.697	22.50	44.99	7.80
20	929.6	1.346	5.379	10.76	1.85	27	214.2	5.918	23.35	46.69	8.10
30	905.1	1.382	5.524	11.05	1.90	28	206.7	6.138	24.19	48.38	8.40
40	881.9	1.418	5.669	11.34	1.95	29	199.7	6.360	25.04	50.07	8.70
50	859.9	1.455	5.814	11.63	2.00	30	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
2°	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
3°	66.67	.39	20'	568.53	28.14	20'	1079.2	100.75
4°	75.01	.49	30'	576.95	28.97	30'	1087.8	102.35
5°	83.34	.61	40'	585.36	29.82	40'	1096.4	103.95
	91.68	.73	50'	593.79	30.68	50'	1105.1	105.60
2 10	100.01	.87	12°	602.21	31.56	22°	1113.7	107.24
20	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
30	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
40	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
50	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3 10	150.04	1.96	13°	652.81	37.07	23°	1165.7	117.38
20	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
30	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
40	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
50	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4 10	200.08	3.49	14°	703.51	43.03	24°	1217.9	128.00
20	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
30	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
40	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
50	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5 10	250.16	5.46	15°	754.32	49.44	25°	1270.2	139.11
20	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
30	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
40	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
50	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6 10	300.28	7.86	16°	805.25	56.31	26°	1322.8	150.71
20	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
30	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
40	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
50	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7 10	350.44	10.71	17°	856.30	63.63	27°	1375.6	162.81
20	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
30	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
40	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
50	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8 10	400.66	13.99	18°	907.49	71.42	28°	1428.6	175.41
20	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
30	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
40	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
50	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9 10	450.93	17.72	19°	958.81	79.67	29°	1481.8	188.51
20	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
30	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
40	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
50	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10 10	501.28	21.89	20°	1010.3	88.39	30°	1535.3	202.12
20	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
30	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
40	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
50	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
31°	1589.0	216.3	41°	2142.2	387.4	51°	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
32°	1643.0	230.9	42°	2199.4	407.6	52°	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
33°	1697.2	246.1	43°	2257.0	428.5	53°	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
34°	1751.7	261.8	44°	2314.9	450.0	54°	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
35°	1806.6	278.1	45°	2373.3	472.1	55°	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.4	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
36°	1861.7	294.9	46°	2432.1	494.8	56°	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
37°	1917.1	312.2	47°	2491.3	518.2	57°	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
38°	1972.9	330.2	48°	2551.0	542.2	58°	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
39°	2029.0	348.6	49°	2611.2	566.9	59°	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
40°	2085.4	367.7	50°	2671.8	592.3	60°	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
62°	3442.7	954.8	72°	4162.8	1352.6	82°	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
63°	3511.1	990.2	73°	4239.7	1398.0	83°	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
64°	3580.3	1026.6	74°	4317.6	1444.6	84°	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
65°	3650.2	1063.9	75°	4396.5	1492.4	85°	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
66°	3720.9	1102.2	76°	4476.5	1541.4	86°	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
67°	3792.4	1141.4	77°	4557.6	1591.6	87°	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
68°	3864.7	1181.6	78°	4639.8	1643.0	88°	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3888.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
69°	3937.9	1222.7	79°	4723.2	1695.8	89°	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
70°	4011.9	1265.0	80°	4807.7	1749.9	90°	5729.7	2373.3
10	4024.4	1272.1	10	4821.7	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20'	5864.6	2469.3	20'	6992.0	3310.2	20'	8388.9	4429.2
30'	5881.7	2481.5	30'	7012.7	3326.1	30'	8415.1	4450.9
40'	5898.8	2493.8	40'	7033.6	3342.3	40'	8441.5	4472.7
50'	5916.0	2506.1	50'	7054.5	3358.5	50'	8468.0	4494.6
92°	5933.2	2518.5	102°	7075.5	3374.9	112°	8494.6	4516.6
10'	5950.5	2531.0	10'	7096.6	3391.2	10'	8521.3	4538.8
20'	5967.9	2543.5	20'	7117.8	3407.7	20'	8548.1	4561.1
30'	5985.3	2556.0	30'	7139.0	3424.3	30'	8575.0	4583.4
40'	6002.7	2568.6	40'	7160.3	3440.9	40'	8602.1	4606.0
50'	6020.2	2581.3	50'	7181.7	3457.6	50'	8629.3	4628.6
93°	6037.8	2594.0	103°	7203.2	3474.4	113°	8656.6	4651.3
10'	6055.4	2606.8	10'	7224.7	3491.3	10'	8684.0	4674.2
20'	6073.1	2619.7	20'	7246.3	3508.2	20'	8711.5	4697.2
30'	6090.8	2632.6	30'	7268.0	3525.2	30'	8739.3	4720.3
40'	6108.6	2645.5	40'	7289.8	3542.4	40'	8767.0	4743.6
50'	6126.4	2658.5	50'	7311.7	3559.6	50'	8794.9	4766.9
94°	6144.3	2671.6	104°	7333.6	3576.8	114°	8822.9	4790.4
10'	6162.6	2684.7	10'	7355.6	3594.2	10'	8851.0	4814.1
20'	6180.2	2697.9	20'	7377.8	3611.7	20'	8879.3	4837.8
30'	6198.3	2711.2	30'	7399.9	3629.2	30'	8907.7	4861.7
40'	6216.4	2724.5	40'	7422.2	3646.8	40'	8936.3	4885.7
50'	6234.6	2737.9	50'	7444.6	3664.5	50'	8965.0	4909.9
95°	6252.8	2751.3	105°	7467.0	3682.3	115°	8993.8	4934.1
10'	6271.1	2764.8	10'	7489.6	3700.2	10'	9022.7	4958.6
20'	6289.4	2778.3	20'	7512.2	3718.2	20'	9051.7	4983.1
30'	6307.9	2792.0	30'	7534.9	3736.2	30'	9080.9	5007.8
40'	6326.3	2805.6	40'	7557.7	3754.4	40'	9110.3	5032.6
50'	6344.8	2819.4	50'	7580.5	3772.6	50'	9139.8	5057.6
96°	6363.4	2833.2	106°	7603.5	3791.0	116°	9169.4	5082.7
10'	6382.1	2847.0	10'	7626.6	3809.4	10'	9199.1	5107.9
20'	6400.8	2861.0	20'	7649.7	3827.9	20'	9229.0	5133.3
30'	6419.5	2875.0	30'	7672.9	3846.5	30'	9259.0	5158.8
40'	6438.4	2889.0	40'	7696.3	3865.2	40'	9289.2	5184.5
50'	6457.3	2903.1	50'	7719.7	3884.0	50'	9319.5	5210.3
97°	6476.2	2917.3	107°	7743.2	3902.9	117°	9349.9	5236.2
10'	6495.2	2931.6	10'	7766.8	3921.9	10'	9380.5	5262.3
20'	6514.3	2945.9	20'	7790.5	3940.9	20'	9411.3	5288.6
30'	6533.4	2960.3	30'	7814.3	3960.1	30'	9442.2	5315.0
40'	6552.6	2974.7	40'	7838.1	3979.4	40'	9473.2	5341.5
50'	6571.9	2989.2	50'	7862.1	3998.7	50'	9504.4	5368.2
98°	6591.2	3003.8	108°	7886.2	4018.2	118°	9535.7	5395.1
10'	6610.6	3018.4	10'	7910.4	4037.8	10'	9567.2	5422.1
20'	6630.1	3033.1	20'	7934.6	4057.4	20'	9598.9	5449.2
30'	6649.6	3047.9	30'	7959.0	4077.2	30'	9630.7	5476.5
40'	6669.2	3062.8	40'	7983.5	4097.1	40'	9662.6	5504.0
50'	6688.8	3077.7	50'	8008.0	4117.0	50'	9694.7	5531.7
99°	6708.6	3092.7	109°	8032.7	4137.1	119°	9727.0	5559.4
10'	6728.4	3107.7	10'	8057.4	4157.3	10'	9759.4	5587.4
20'	6748.2	3122.9	20'	8082.3	4177.5	20'	9792.0	5615.5
30'	6768.1	3138.1	30'	8107.3	4197.9	30'	9824.8	5643.8
40'	6788.1	3153.3	40'	8132.3	4218.4	40'	9857.7	5672.3
50'	6808.2	3168.7	50'	8157.5	4239.0	50'	9890.8	5700.9
100°	6828.3	3184.1	110°	8182.8	4259.7	120°	9924.0	5729.7
10'	6848.5	3199.6	10'	8208.2	4280.5	10'	9957.5	5758.6
20'	6868.8	3215.1	20'	8233.7	4301.4	20'	9991.0	5787.7
30'	6889.2	3230.8	30'	8259.3	4322.4	30'	10025.0	5817.0
40'	6909.6	3246.5	40'	8285.0	4343.6	40'	10059.0	5846.5
50'	6930.1	3262.3	50'	8310.8	4364.8	50'	10093.0	5876.1

Table V. Corrections for use with Table IV,

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ANGLE	For Tangents Add													
	CURVE 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.20	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.49	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34

For Externals Add

ANGLE	CURVE 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.054
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.618	.707	.797	.877	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	1/2 sub chord R = sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

CURVE FORMULAS.

$T = R \tan \frac{1}{2} I$	$R = T \cot. \frac{1}{2} I$	Chord def. = $\frac{\text{chord}^2}{R}$
$T = \frac{50 \tan. \frac{1}{2} I}{\text{Sin. } D}$	$R = 50 \frac{\text{Sin. } D}{\text{Sin. } I}$	No. chords = $\frac{1}{2} \frac{I}{D}$
$\text{Sin. } D = \frac{50}{R}$	$E = R \text{ ex. sec. } \frac{1}{2} I$	Tan. def. = $\frac{1}{2} \text{ chord def.}$
$\text{Sin. } D = \frac{50 \tan. \frac{1}{2} I}{T}$	$E = T \tan \frac{1}{2} I$	

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.— Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10. $10^2 \div 200 = .5$. $100 + .5 = 100.5$ hyp.

Given Hyp. 100, Alt. 25. $25^2 \div 200 = 3.125$. $100 - 3.125 = 96.875 =$ Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

Natural Sines

DEG.	0'	10'	20'	30'	40'	50'	DEG.	DEG.	0'	10'	20'	30'	40'	50'	DEG.
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1276	1305	1334	1363	82	47	7314	7334	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7717	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10
DEG.	60'	50'	40'	30'	20'	10'	DEG.	DEG.	60'	50'	40'	30'	20'	10'	DEG.
DEG.	0'	10'	20'	30'	40'	50'	DEG.								
80	9848	9853	9858	9863	9868	9872	9								
81	9877	9881	9886	9890	9894	9898	8								
82	9903	9907	9911	9914	9918	9922	7								
83	9925	9929	9932	9936	9939	9942	6								
84	9945	9948	9951	9954	9957	9959	5								
85	9962	9964	9967	9969	9971	9974	4								
86	9976	9978	9980	9981	9983	9985	3								
87	9986	9988	9989	9990	9992	9993	2								
88	9994	9995	9996	9997	9997	9998	1								
89	9998	9999	9999	9999	1.0000	1.0000	0								
DEG.	60'	50'	40'	30'	20'	10'	DEG.								

Natural Cosines

Natural Tangents

deg.	0'	10'	20'	30'	40'	50'	deg.	0'	10'	20'	30'	40'	50'	deg.	
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8667	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10
deg.	60'	50'	40'	30'	20'	10'	deg.	60'	50'	40'	30'	20'	10'	deg.	

deg.	0'	10'	20'	30'	40'	50'	deg.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.524	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.770	0
deg.	60'	50'	40'	30'	20'	10'	deg.

Natural Cotangents

136
82
53

108+60 Fr drain West

109+15 " " "

14+20 both sides



1420 470
 4
 56.80
 630

607d
 35.26

2.08
 95
 1.43

1109
 11098

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER
 DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE SIDE SLOPES 1:1
 FOR STREET TRACK ENGINEERING
 CHARDON O.
 PHONE 250-X

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

109795
 1260
 1110.61

MADE IN GERMANY.

R.

